



CONSULTING ENGINEERS, CORP.
ENGINEERING CONSULTANTS

Design Guide
For
AmDeck Floor and Roof System

December 07, 2007



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Client: Amvic, Inc.

Prepared by: Kapil
Checked by: Andy / Raj

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1 Exemptions (Disclaimer)

The information given in this document is based on engineering design principles as set forth in ACI 318-02 (Building Code Requirements for Structural Concrete) for one way concrete joist.

This document shall only be used by Registered Architects/ Professional Engineers who possess the required credentials and who are competent to evaluate the significance and limitations of the information provided herein.

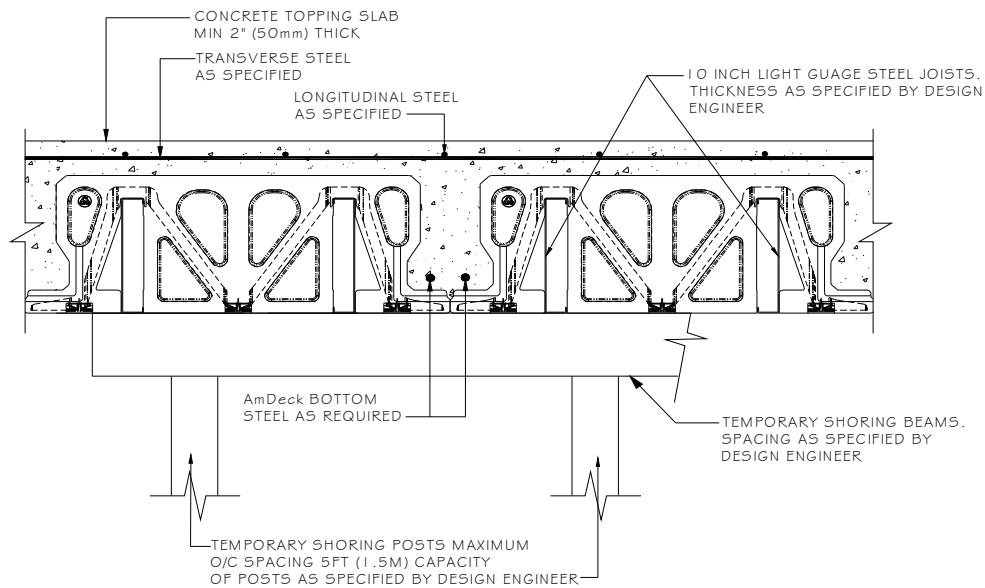
The Registered Architects/ Professional Engineers using this document to specify the AmDeck ® system for a specified project is solely responsible for determining that the project loads, span lengths, span configurations, connection details are in full compliance and within the limitations stated in this reports.

2 Scope of Work

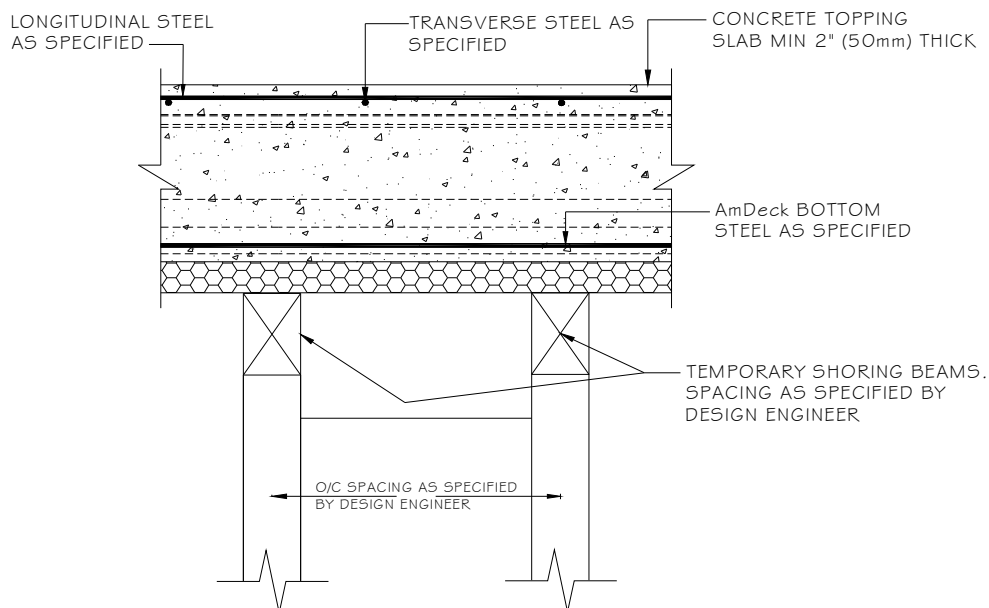
- i. The Review and analysis of the AmDeck floor and roof systems information has been provided by Amvic. [Six (6) different floor configuration with 12" panel depth & topping slabs varying from 2" to 4½" in ½" increment were analyzed and designed.]
- ii. EACH Amvic floor configuration analyzed and designed for:-
 - Uniform dead load of 10 psf and 15 psf.
 - Uniform live load of 40 psf to 100 psf in 10 psf increment.
 - 3500 psi and 4000 psi compressive strength of co concrete were considered.
 - ACI 318 – 02 and IBC – 2003 Codes has been used for analysis and design.
- iii. Temporary shoring spans are designed and provided in tabular form.
- iv. Design guide table for various design parameters including reinforcement design and spans has been provided.

3 Introduction

The **AmDeck® Floor & Roof System** consists of modular, lightweight stay-in-place forms made of Expanded Polystyrene (EPS) that is used to construct floors & roofs. The system utilizes 10 inch deep lightweight steel framing stud embedded in the floor form work (refer typical transverse section) to carry temporary construction loads and to acts as furring strips for interior finishing.



TYPICAL TRANSVERSE SECTION



TYPICAL LONGITUDINAL SECTION

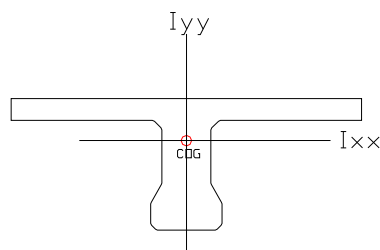
4 Am Deck Joist Design Criteria

Panel Designation	=	12" Panel section with 10" beam
Beam Depth	=	d_w in inches
Topping	=	t_f in inches
Minimum Beam Width, bottom	=	b_w in inches
Average Joist Width	=	b_{wa} in inches
Panel Span, Transverse	=	b in inches
Maximum Span of the Deck	=	L in feet & inches
Number of Span	=	Single (SS) / Double (DS) / Multiple (MS)
Live load acting on the deck	=	w_{LL} in psf
Dead load acting on the deck	=	w_{DL} in psf
Unit weight of concrete	=	γ_c in pcf
Specified compressive strength of concrete	=	f'_c in psi
Yield strength of rebar	=	f_y in psi
Rebar cover, Center of rebar	=	c in inches
Allowable Deflection factor, Total	=	$\Delta_{Factor Total}$
Allowable Deflection factor, LL	=	$\Delta_{Factor LL}$

4.1 Assumptions

- i. Design criteria are based on **IBC 2003 + ACI 318-02** codes.
- ii. Modulus of elasticity of rebar is assumed to be 29000 ksi for the design.
- iii. 'Normal weight concrete' is assumed to be used in wall construction and therefore $\lambda = 1.0$ corresponding to 'Normal weight concrete' has been use in design.
- iv. Factored load combination of $1.2DL + 1.6LL$ is used in strength calculation & service load $DL + LL$ is used in deflection calculation.
- v. 'AmDeck floor system' is of type 'Concrete joist construction' as specified in code.

4.2 Analysis



TYPICAL CROSS SECTION

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$$\text{Dead Load factor} = K_{DL}$$

$$\text{Live Load factor} = K_{LL}$$

Section Properties

Cross-section area of Combined Section (A) = As Provided by Amvic (Refer Table below)
Distance of CG from top (CG_{Top}) = As Provided by Amvic (Refer Table below)
Moment of inertia about x-axis (I_{XX}) = As Provided by Amvic (Refer Table below)
Section Modulus about x-axis (S_{XX}) = $I_{XX} / (\text{Max } (CG_{Top}, (d_w + t_f - CG_{Top})))$

Topping (inch)	Area (in ²)	Perimeter (inch)	I _{xx} (in ⁴)	I _{yy} (in ⁴)	R _x (inch)	R _y (inch)	Cg _{Top} (inch)	Cg _{Bottom} (inch)
2	115.9922	88.9652	1632.1071	5587.8915	3.7511	6.941	3.8451	8.1549
2.5	131.9922	89.9652	1868.2302	6953.2249	3.7622	7.258	3.8487	8.6513
3.0	147.9922	90.9652	2108.2903	8318.5582	3.7744	7.497	3.9056	9.0944
3.5	163.9922	91.9652	2357.9644	9683.8916	3.7919	7.685	4.001	9.4999
4.0	179.9922	92.9652	2621.6218	11049.2249	3.8164	7.835	4.1223	9.8777
4.5	195.9922	93.9652	2902.8583	12414.558	3.8485	7.959	4.2654	10.2346
5.0	211.9922	94.9652	3204.7879	13779.8915	3.8881	8.062	4.4246	10.5754

$$\text{Effective depth } (d) = d_w - c + t_f$$

$$\text{Self weight of deck } (w_{Self}) = w_C \times A / 144$$

$$\text{Total Dead Load } W_{DTotal} = w_{Self} + w_{DL} \times b / 12$$

$$\text{Live Load } W_{LL} = w_{LL} \times b / 12$$

$$\text{Total Unfactored Load } W_P = w_{DTotal} + W_{LL}$$

$$\text{Total factored load } (P_U) = \{K_{DL} \times W_{DTotal} + K_{LL} \times W_{LL}\}$$

ACI318-02 Section 8.3.3 followed for following approximate Shear & Moment in Joist

$$\text{Maximum Shear Force } (V_U) = P_U \times L / 2 \quad \{\text{For Single \& Double Span}\}$$

$$= 1.15P_U \times L / 2 \quad \{\text{For Multiple Span}\}$$

$$\text{Maximum Positive Moment } (M_{UP})$$

$$= (P_U \times L^2 / 8) \times 12 \quad \{\text{For Single Span}\}$$

$$= (P_U \times L^2 / 14) \times 12 \quad \{\text{At End Spans of Double \& Multiple Span}\}$$

$$= (P_U \times L^2 / 16) \times 12 \quad \{\text{At Interior Spans of Multiple Span}\}$$

$$\text{Maximum Negative Moment } (M_{UN})$$

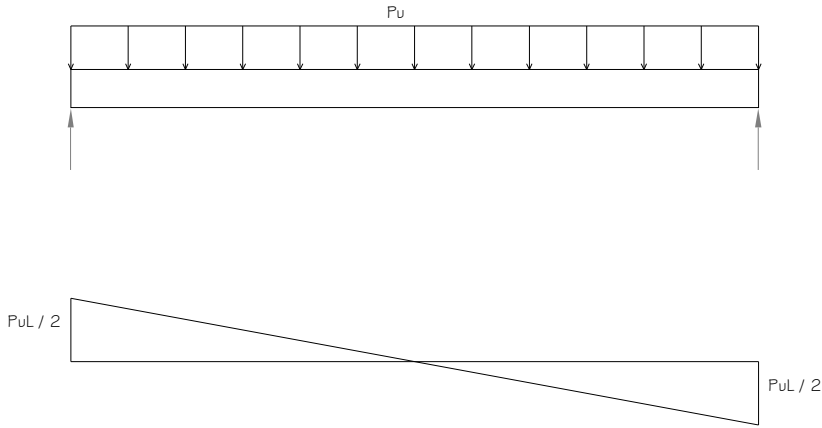
$$= 0 \quad \{\text{For Single Span}\}$$

$$= (P_U \times L^2 / 16) \times 12 \quad \{\text{At Exterior Support of Double \& Multiple Span}\}$$

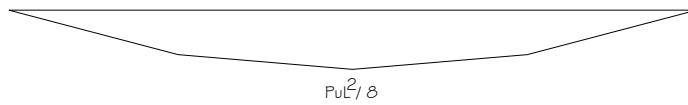
$$= (P_U \times L^2 / 9) \times 12 \quad \{\text{At 1st Interior Support of Double Span}\}$$

$$= (P_U \times L^2 / 10) \times 12 \quad \{\text{At 1st Interior Support of Multiple Span}\}$$

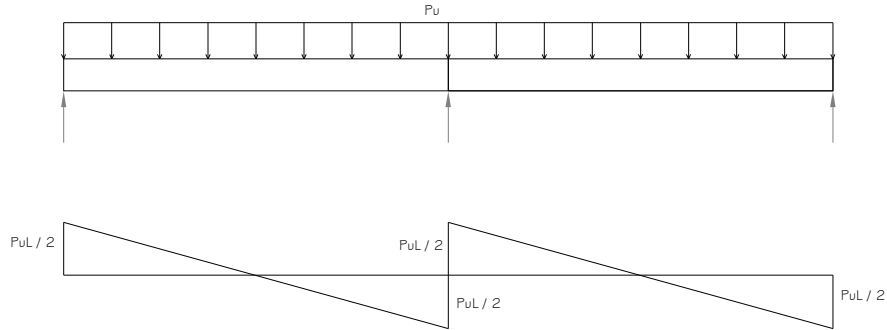
$$= (P_U \times L^2 / 11) \times 12 \quad \{\text{At Other Interior Support of Multiple Span}\}$$



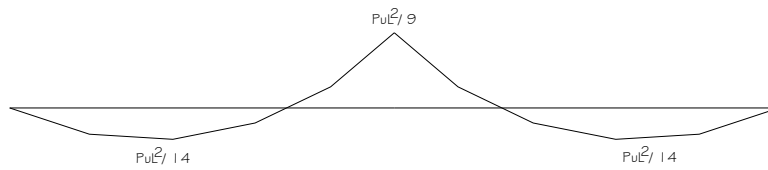
SHEAR FORCE DIAGRAM FOR SINGLE SPAN



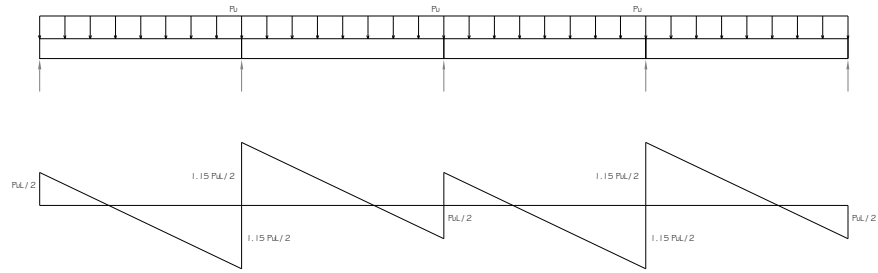
BENDING MOMENT DIAGRAM FOR SINGLE SPAN



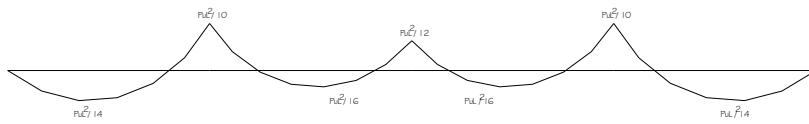
SHEAR FORCE DIAGRAM FOR DOUBLE SPAN



BENDING MOMENT DIAGRAM FOR DOUBLE SPAN



SHEAR FORCE DIAGRAM FOR MULTIPLE SPAN



BENDING MOMENT DIAGRAM FOR MULTIPLE SPAN

4.3 Design

4.3.1 Shear Strength

$$\text{Shear Strength of the section } (\phi V_c) = 1.1 \times 0.75 \times 2 \times (f'c)^{0.5} \times b_w \times d \text{ (Per Section 8.11.8 \& 11.3 of ACI - 318-02)}$$

If $\phi V_c < V_U$, Provide Single leg stirrup rebar and provide corresponding rebar at top to support stirrups.

{

$$\text{Area of single leg rebar stirrup} = A_V \text{ in}^2$$

$$\text{Spacing of stirrup rebar} = S_S \text{ in}$$

$$\text{Shear strength provided by shear reinforcement } (\phi V_S) = 0.75 \times A_V \times f_y \times d / S_S$$

$$\text{Total Shear strength } (\phi V_N) = \phi V_c + \phi V_S \text{ (Per Section 11.1 of ACI - 318-02)}$$

4.3.2 Moment Strength

$$\text{Strength reduction factor } (\phi) = 0.9$$

$$\beta_1 = \begin{cases} 0.85 & \text{if } (f'c \leq 4000 \text{ psi}) \\ 0.80 & \text{if } (4000 < f'c \leq 5000 \text{ psi}) \\ 0.75 & \text{if } (5000 < f'c \leq 6000 \text{ psi}) \\ 0.65 & \text{if } (6000 < f'c) \end{cases}$$

(Above Values are per Table 6-1 of "Notes on ACI 318-02")

$$\text{Balanced reinforcement ratio } (\rho_t) = 0.319 \times \beta_1 \times f'c / f_y$$

$$\text{Maximum allowed reinforcement ratio } (\rho_{Max}) = \rho_t$$

$$\text{Minimum reinforcement ratio } (\rho_{Min}) = \text{Max } (3 \times (f'c)^{0.5}, 200) / f_y$$

Positive Reinforcement

$$\text{Reinforcement ratio for +ive moment } (\rho_{Pos})$$

$$= (0.85 \times f'c / f_y) \times \{1 - [1 - 2 \times M_{UP} / (\phi \times b_w \times d^2 \times 0.85 \times f'c)]^{0.5}\}$$

$$\text{Area of reinforcement required } (A_{S \text{ Pos req}}) = \rho_{Pos} \times b_w \times d$$

$$A_{S \text{ Pos provided}} > A_{S \text{ Pos required}}$$

Negative Reinforcement (For Span > 1)

$$\text{Reinforcement ratio for -ive moment } (\rho_{Neg})$$

$$= (0.85 \times f'c / f_y) \times \{1 - [1 - 2 \times M_{UN} / (\phi \times b_w \times d^2 \times 0.85 \times f'c)]^{0.5}\}$$

$$\text{Area of reinforcement required } (A_{S \text{ Neg req}}) = \rho_{Neg} \times b_w \times d$$

$$A_{S \text{ Neg provided}} > A_{S \text{ Neg required}}$$

Nominal moment strength

Plain Concrete

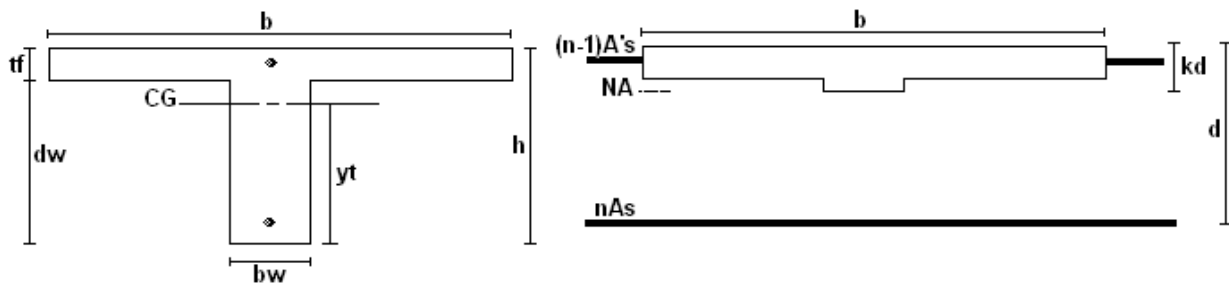
Nominal moment strength of the section (ϕMn) = $0.65 \times 5 (f'c)^{0.5} \times S_{XX}$

Reinforced Concrete

Nominal moment strength of the section (ϕMn)
 = $\phi A_{S \text{ Pos provided}} \times f_y \times [d - (A_{S \text{ Pos provided}} \times f_y / (0.85 \times f'c \times b))/2]$

4.3.3 Deflection

- Total depth of section (h) = $d_w + t_f$
- A_{LP} = $A_{S \text{ Neg provided}}$
- A_B = $A_{S \text{ Pos provided}}$
- R_{DS} = Diameter of shear rebar
- R_{DLP} = Diameter of Single rebar $A_{S \text{ Neg provided}}$
- Effective depth (d_{LP}) = $d_w + t_f - c - R_{DS} - 0.5R_{DLP}$
- Modulus of elasticity of concrete (E_C) = $(\gamma_C)^{1.5} \times (33 \times (f'c)^{0.5})$
- Modular ratio (n) = E_S / E_C
- Modulus of rupture of concrete (f_r) = $7.5 \times (f'c)^{0.5}$



Gross Section

Cracked Transformed Section

- y_t = Cg_{Bottom} As Provided by Amvic (Refer Table above)
- I_g = I_{XX} As Provided by Amvic (Refer Table above)
- Cracking Moment (M_{CR}) = $f_r \times I_g / y_t$
- C = $b_w / (n \times A_{S \text{ Pos provided}})$
- f = $t_f \times (b - b_w) / (n \times A_{S \text{ Pos provided}})$
- r = $(n - 1) A_{S \text{ Neg provided}} / (n A_{S \text{ Pos provided}})$
- d' = $h - d_{LP}$

$kd = \frac{\sqrt{C(2d + t_f \times f + 2rd') + (f + r + 1)^2} - (f + r + 1)}{C}$ (Per Table 10-2 of "Notes on ACI318-02")

Moment of inertia of cracked section transformed to concrete (I_{cr})

$= (b - b_w)t_f^3 / 12 + b_w(kd)^3 / 3 + (b - b_w)t_f(kd - t_f / 2)^2 + nA_{Bi}(d - kd)^2 + (n - 1)A_{LPi}(kd - d')^2$
 (Per Table 10-2 of "Notes on ACI318-02")

Service Moment (M_P)

$$\text{Dead Load moment, } M_D = W_{D \text{ Total}} \times L^2 / 8$$

$$\text{Live Load moment, } M_L = W_{LL} \times L^2 / 8$$

$$\text{Total moment, } M_{D+L} = M_D + M_L$$

$$\text{Sustained Moment, } M_{SUS} = M_D + 0.5 \times M_L \quad (\text{Assuming that 50\% of Live Load as sustained load})$$

Effective moment of inertia for deflection computation (I_e)

$$= I_g \quad \text{if } M_{CR} > M_P$$

$$= \text{Min. of } [\{ (M_{CR} / M_P)^3 I_g + [1 - (M_{CR} / M_P)^3] I_{CR} \} \text{ and } I_g] \text{ if } M_{CR} \leq M_P$$

4.3.3.1 Short Term Deflection

For Continuous beam, the mid-span deflection $\Delta_i = K (5/48) M_P \times L^2 / (E_c \times I_e)$
(Per Section 9.5.2.4 of "Notes on ACI318-02")

Where,

$$\begin{aligned} K &= 1.20 - 0.20 M_P / M_O \text{ for continuous beam} \\ &= 0.80 \text{ for Continuous fixed-hinged beam, mid span deflection} \\ &= 0.738 \text{ for Continuous fixed-hinged beam, maximum deflection using} \\ &\quad \text{maximum moment} \\ &= 0.60 \text{ for fixed-fixed beam} \\ &= 1.0 \text{ for Simple Beam} \end{aligned}$$

$$M_O = \text{Simple span moment at mid span, } = (P \times L^2 / 8) \times 12$$

Use $K = 1.0$ to be on conservative side

$$\Delta_{iD} = K (5/48) M_D \times L^2 / (E_c \times I_e)$$

$$\Delta_{iLL} = K (5/48) M_{LL} \times L^2 / (E_c \times I_e)$$

$$\Delta_{iSUS} = K (5/48) M_{SUS} \times L^2 / (E_c \times I_e)$$

$$\Delta_{iTotal} = \Delta_{iD} + \Delta_{iLL}$$

Allowable Short Term Deflections

$$\Delta_{i \text{ Allow LL}} = (L \times 12) / (\Delta_{\text{Factor LL}})$$

4.3.3.2 Long Term Deflection

$$\Delta_{(CP+SH)} = \lambda \times \Delta_{iSUS} \quad (\text{Per Section 9.5.2.5 of "Notes on ACI318-02"})$$

Where

$$\lambda = \xi / (1 + 50p')$$

$$p' = \text{Area of compression steel } (A') / (b_w \times d)$$

$$\xi = \text{Time- dependent factor}$$

$$= 2.0 \quad \text{5 years and more Sustained load duration}$$

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$$= 1.4 \quad 12 \text{ months}$$

$$= 1.2 \quad 6 \text{ months}$$

$$= 1.0 \quad 3 \text{ months.}$$

$$\Delta_{LT} = \Delta_{(CP+SH)} + \Delta_{iLL}$$

Allowable Long Term Deflection

$$\Delta_{i \text{ Allow LL}} = (L \times 12) / (480 \text{ or } 240)$$

5 Slab Reinforcement Design Criteria

5.1 Transverse Reinforcement

$$L_{\text{Slab}} = b/12$$

$$M_{u \text{ Slab}} = P_u \times L_{\text{Slab}}^2 / 12$$

$$\text{Balanced reinforcement ratio } (\rho_t) = 0.319 \times \beta_1 \times f'_c / f_y \quad (\text{Per Section 7.1 of Notes on ACI 318-02})$$

$$\text{Maximum allowed reinforcement ratio } (\rho_{\text{Max}}) = \rho_t$$

$$\text{Minimum reinforcement ratio } (\rho_{\text{Min}}) = \text{Max } (3 \times (f'_c)^{0.5}, 200) / f_y \quad (\text{Per Section 10.5.1 ACI 318-02})$$

$$\text{Reinforcement ratio for +ive moment } (\rho_{\text{Pos}})$$

$$= (0.85 \times f'_c / f_y) \times \{1 - [1 - 2 \times M_{UP} / (\phi \times b_w \times t_f / 2^2 \times 0.85 \times f'_c)]^{0.5}\}$$

$$\text{Area of reinforcement required } (A_{S \text{ Pos req}}) = \rho_{\text{Pos}} \times 12 \times t_f / 2$$

$$\text{Area of reinforcement required } (A_{S \text{ Pos req}}) \text{ (Minimum)} = \rho_{\text{Min}} \times 12 \times t_f / 2$$

$$\text{Area of reinforcement required } (A_{S \text{ Pos req}}) \text{ (Maximum)} = \rho_{\text{Max}} \times 12 \times t_f / 2$$

$$\text{If } A_{S \text{ Pos req}} \text{ (Minimum)} > A_{S \text{ Pos req}}$$

$$\text{Then Provided Area of Steel} = \text{Minimum of } A_{S \text{ Pos req}} \text{ (Minimum) or } 1.33 \times A_{S \text{ Pos req}}$$

$$\text{If } A_{S \text{ Pos req}} \text{ (Minimum)} \leq A_{S \text{ Pos req}}$$

$$\text{Then Provided Area of Steel} = A_{S \text{ Pos req}}$$

$$\text{Minimum Spacing, } S_{\text{Calculated}} = (A_{\text{rebar}} / \text{Area of Steel Provided}) \times 12$$

However per section 7.12 of ACI 318-02, minimum spacing will be lesser of following three

- (1) $S_{\text{Calculated}}$
- (2) 18" O.C.
- (3) $5 \times t_f$ (t_f is thickness of slab)

5.2 Longitudinal Reinforcement

Minimum Longitudinal reinforcement as per section 7.12 of ACI 318-02 to be calculated by following equation.

$$\text{For Grade 60 rebar, } A_s \text{ Minimum} = 0.0018 \times \text{Cross sectional Area}$$

$$\text{Spacing for } A_s \text{ Minimum, } S_{\text{Calculated}} = (A_{\text{rebar}} / \text{Area of Steel Provided}) \times 12$$

However per section 7.12 of ACI 318-02, minimum spacing will be lesser of following three

- (1) $S_{\text{Calculated}}$
- (2) 18" O.C.
- (3) $5 \times t_f$ (t_f is thickness of slab)

6 Shoring Design Criteria

Joist Spacing	=	16"
Self weight of joist	=	(Area of Joist/ 2 x Unit wt. of concrete)/144
Self weight of topping	=	(16 x topping thickness x Unit wt. of concrete) /144
Total dead load	=	Self weight of joist + Self weight of topping
Construction Load	=	Joist Spacing x W_{LL} / 12
Self weight of steel joist	=	$W_{DL \text{ Steel}}$
Total Load, W	=	Total Dead Load + Construction load + Self wt. of steel joist

Maximum Allowed span

Based on Allowable Moment

Joist Designation	UNPERFORATED PROPERTIES									PERFORATED PROPERTIES				
	Mrx (in.kip)	Lu (in)	Mry web.comp. (in.kip)	Mry lips.comp. (in.kip)	Shear Vr (kips)	Web Cripp Pr (kips)	Ix (in ⁴)	Iy (in ⁴)	Sf (in ³)	Mrx (in.kip)	Mry web.comp. (in.kip)	Mry lips.comp. (in.kip)	Shear Vr (kips)	Ix def. (in ⁴)
1000S162-54	70.7	31.3	6.39	6.96	2.12	1.1	9.95	0.205	1.99	70.7	5.99	6.89	2.12	9.31
1000S162-68	96.9	31	7.95	8.4	4.27	1.67	12.3	0.247	2.47	96.9	7.51	8.32	4.27	11.9
1000S162-97	147	30.4	10.7	10.9	12.6	3.17	17	0.321	3.39	147	10.3	10.8	9.17	17

Allowable moment	=	M_{Max} from Amvic chart (Refer Table)
M_{Max}	=	$W \times L^2 / 8$
L	=	$\sqrt{(M_{Max} \times 8 / W)}$

Based on Allowable shear

V_x	=	$W \times L / 2$
L	=	$2 \times V_x / W$

Based on Deflection factor

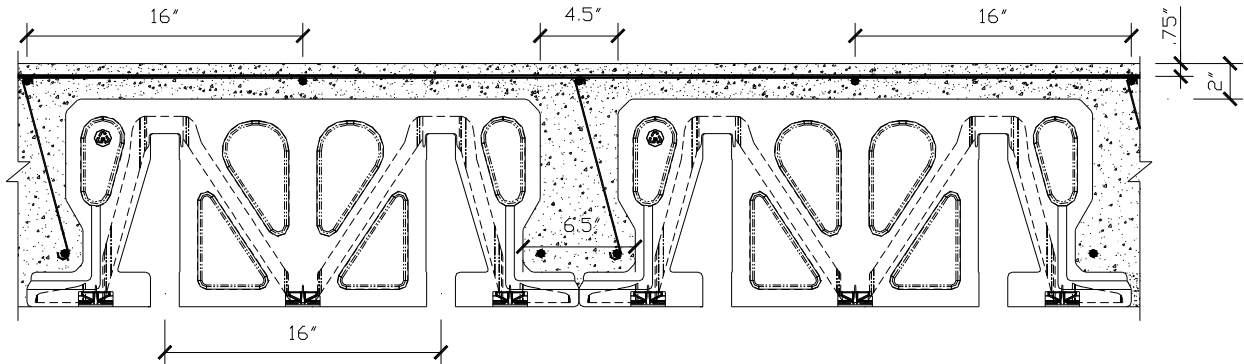
Allowable deflection, ADF	=	L/ Deflection factor (D_F)
ADF	=	$L / \text{Deflection factor } (D_F) = \frac{5}{384} \times \frac{W \times L^4}{E \times I}$
L	=	$\sqrt[3]{\Delta \times \frac{384}{5} \times \frac{E \times I}{W}}$

Based on Crippling

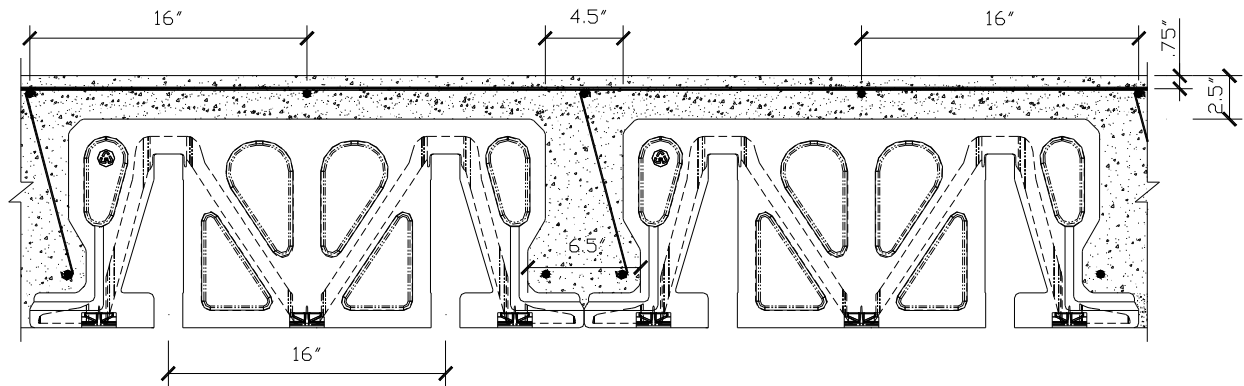
Web Crippling Load, P_r	=	$W \times L / 2$
Span of Shoring	=	Minimum of (L_{Moment} , L_{Shear} , $L_{\text{Deflection}}$ & $L_{\text{Crippling}}$)

7 Specifications

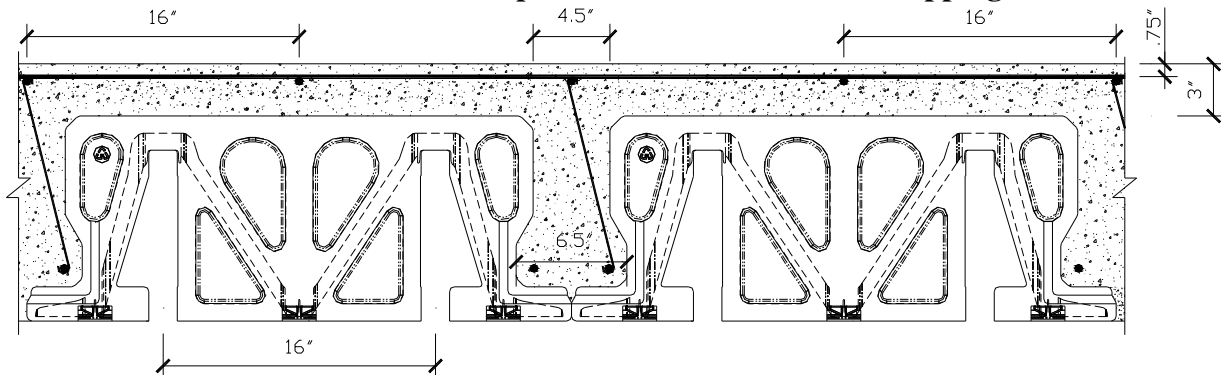
i. **12" Panel Size With 10" Deep Joist @ 32" O.C. And 2" Topping Slab**



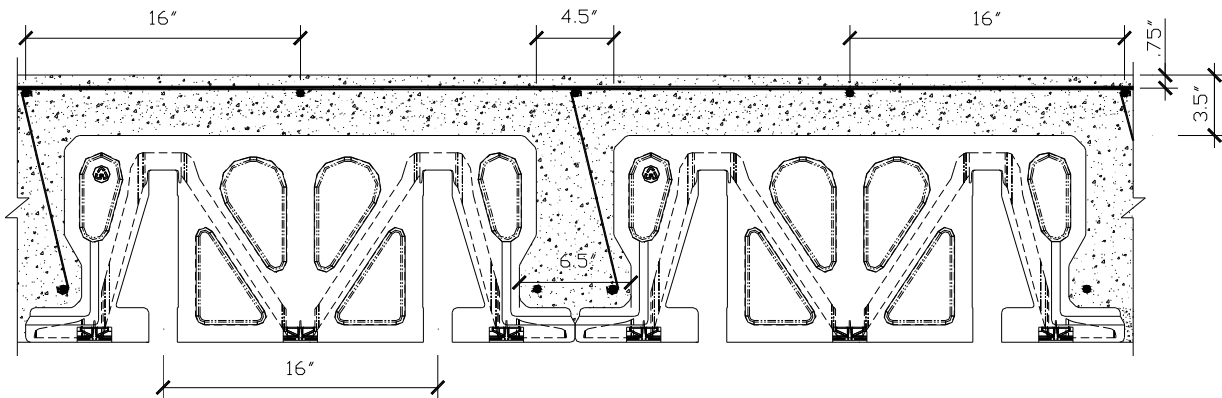
ii. **12" Panel Size With 10" Deep Joist @ 32" O.C. And 2.5" Topping Slab**



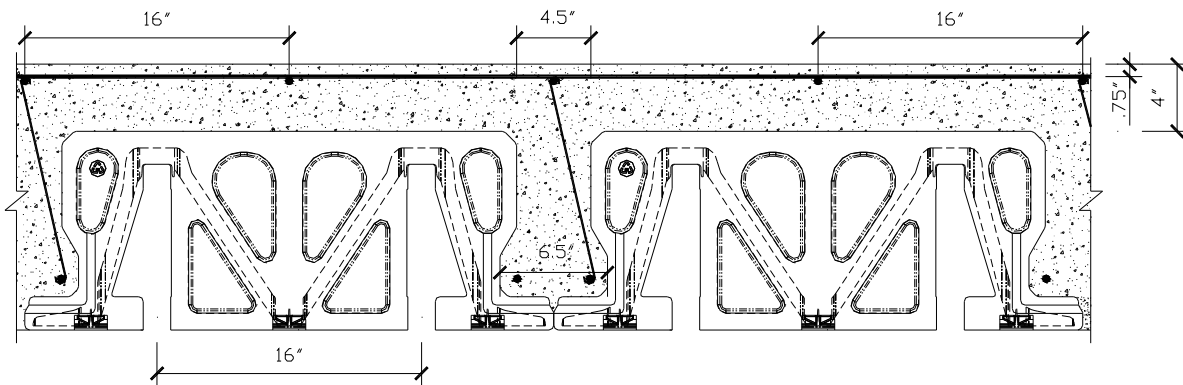
iii. **12" Panel Size With 10" Deep Joist @ 32" O.C. And 3" Topping Slab**



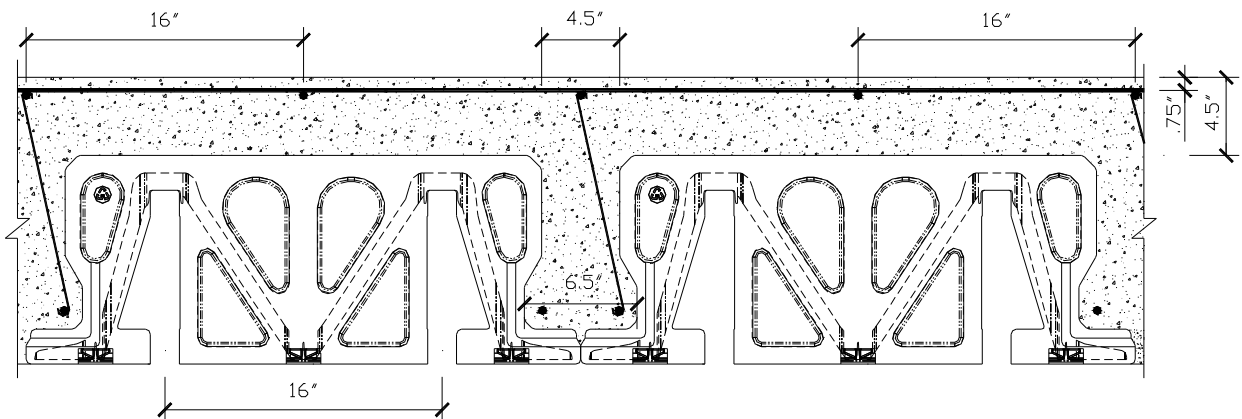
iv. 12" Panel Size With 10" Deep Joist @ 32" O.C. And 3.5" Topping Slab



v. 12" Panel Size With 10" Deep Joist @ 32" O.C. And 4" Topping Slab



vi. 12" Panel Size With 10" Deep Joist @ 32" O.C. And 4.5" Topping Slab



8 AmDeck Joist Design Calculations

8.1 Single Span Joist

(12" Panel Size With 10" Deep Joist @ 32" O.C. And 2" Topping Slab)

8.1.1 Inputs

Panel Designation	=	12" Panel section with 10" deep beam
Beam Depth (dw)	=	10"
Topping (t _f)	=	2"
Minimum Beam Width, bottom (b _w)	=	6.5"
Average Joist Width (b _{wa})	=	5.2"
Panel Span, Transverse (b)	=	32"
Maximum Span of the Deck (L)	=	10'-0"
Number of Span	=	Single
Live load acting on the deck (w _{LL})	=	40 psf
Dead load acting on the deck (w _{DL})	=	10 psf
Unit weight of concrete (γ _c)	=	145 pcf
Specified compressive strength of concrete (f' _c)	=	3500 psi
Yield strength of rebar (f _y)	=	60000 psi
Rebar cover, Center of rebar (c)	=	1.25"
Allowable Deflection factor, Total (Δ _{Factor LL})	=	180 (Short Term)
Allowable Deflection factor, Total (Δ _{Factor LL})	=	240 (Long Term)

8.1.2 Analysis

Dead Load factor (K _{DL})	=	1.2
Live Load factor (K _{LL})	=	1.6

Section Properties

Cross-section area A	=	115.9888 in ² (Refer Table on Page – 7)
Distance of CG from top (CG _{Top})	=	3.8451 in from top
Moment of inertia about x-axis (I _{XX})	=	1632.1 in ⁴
Section Modulus about x-axis (S _{XX})	=	1632.1 / {Max [3.8451, (10 + 2 – 3.8451)]}
	=	200.137 in ³
Effective depth (d)	=	d _w – c + t _f
	=	10 – 1.25 + 2
	=	10.75"
Self weight of deck (w _{Self})	=	w _C × A _{Gross}
	=	145 × 115.9888/144

$$\begin{aligned}
 &= 116.794 \text{ plf} \\
 \text{Total Dead Load } W_{D\text{Total}} &= \text{Self Weight} + \text{Applied Additional Dead Load} \\
 &= 116.794 + 10 \times 32/12 \\
 &= 143.46 \text{ plf} \\
 \text{Live Load } W_{LL} &= 40 \times 32/12 \\
 &= 106.67 \text{ plf} \\
 \text{Total Unfactored Load } W_P &= W_{D\text{Total}} + W_{LL} \\
 &= 143.46 + 106.67 \\
 &= 250.13 \text{ plf} \\
 \text{Total factored load } (P_U) &= \{K_{DL} \times W_{D\text{Total}} + K_{LL} \times W_{LL}\} \\
 &= 1.2 \times 143.46 + 1.6 \times 106.67 \\
 &= 342.824 \text{ plf} \\
 \text{Maximum Shear Force } (V_U) &= P_U \times L / 2 \\
 &= 342.824 \times 10 / 2 \\
 &= 1714.12 \text{ lb.} \\
 \text{Maximum Positive Moment } (M_{UP}) &= (P_U \times L^2 / 8) \times 12 \\
 &= (342.824 \times 10^2 / 8) \times 12 \\
 &= 51423.6 \text{ in-lb.} \\
 \text{Maximum Negative Moment } (M_{UN}) &= 0
 \end{aligned}$$

8.1.3 Design

8.1.3.1 Shear Strength

$$\begin{aligned}
 \text{Shear Strength of the section } (\phi V_c) &= 1.1 \times 0.75 \times 2 \times (f'c)^{0.5} \times b_{wa} \times d \\
 &= 1.1 \times 0.75 \times 2 \times (3500)^{0.5} \times 5.2 \times 10.75 \\
 &= \mathbf{5456.69 \text{ lb.} > V_U (= 1714.12 \text{ lb.})} \quad \text{(OK)}
 \end{aligned}$$

8.1.3.2 Moment Strength

$$\begin{aligned}
 \text{Strength reduction factor } (\phi) &= 0.9 \\
 \beta_1 &= \begin{cases} 0.85 & \text{if } (f'c \leq 4000 \text{ psi}) \\ 0.80 & \text{if } (4000 < f'c \leq 5000 \text{ psi}) \\ 0.75 & \text{if } (5000 < f'c \leq 6000 \text{ psi}) \\ 0.65 & \text{if } (6000 < f'c) \end{cases} \\
 \beta_1 &= 0.85 \quad \text{since } (f'c \leq 4000 \text{ psi}) \\
 \text{Tension controlled reinforcement ratio } (\rho_t) &= 0.319 \times 0.85 \times 3500 / 60000 \\
 &= 0.0158 \\
 \text{Maximum allowed reinforcement ratio } (\rho_{\text{Max}}) &= \rho_t \\
 &= 0.0158 \\
 \text{Minimum reinforcement ratio } (\rho_{\text{Min}}) &= \text{Max } (3 \times (f'c)^{0.5}, 200) / f_y \\
 &= \text{Max } (3 \times (3500)^{0.5}, 200) / 60000 \\
 &= \text{Max } (177.5, 200) / 60000
 \end{aligned}$$

$$= 200 / 60000$$

$$= 0.0033$$

Positive Reinforcement

Reinforcement ratio for +ive moment (ρ_{Pos})

$$= (0.85 \times f'c / fy) \times \{1 - [1 - 2 \times M_{UP} / (\phi \times b_{wa} \times d^2 \times 0.85 \times f'c)]^{0.5}\}$$

$$= (0.85 \times 3500 / 60000) \{1 - [1 - 2 \times 51423.6 / (0.9 \times 5.2 \times 10.75^2 \times 0.85 \times 3500)]^{0.5}\}$$

$$= 0.00161 < (\rho_{Min} = 0.0033)$$

$$= 0.0033 < (\rho_{Max} = 0.0158) \text{ OK}$$

Area of reinforcement required ($A_{S_{Pos}} \text{ req}$) = $\rho_{Pos} \times b_{wa} \times d$

$$= 0.0033 \times 5.2 \times 10.75$$

$$= 0.18847 \text{ in}^2$$

$A_{S_{Pos}}$ provided = 1 # 4 (Area = 0.1963 in² > 0.18847) **OK**

Nominal moment strength

Plain Concrete

Nominal moment strength of the section (ϕM_n) = $0.65 \times 5 (f'c)^{0.5} \times S_{XX}$

$$= 0.65 \times 5 \times (3500)^{0.5} \times 200.137$$

$$= 38480.86 \text{ in-lb.}$$

Reinforced Concrete

Nominal moment strength of the section (ϕM_n)

$$= \phi A_{S_{Pos}} \text{ provided} \times fy \times [d - (A_{S_{Pos}} \text{ provided} \times fy / (0.85 \times f'c \times b))/2]$$

$$= 0.9 \times 0.1963 \times 60000 \times [10.75 - (0.1963 \times 60000 / (0.85 \times 3500 \times 32))/2]$$

$$= 113296.43 \text{ in-lb.}$$

8.1.3.3 Deflection

Total depth of section (h) = $d_w + t_f$

$$= 10 + 2$$

$$= 12''$$

$$A_{LP} = 0 \text{ in}^2$$

$$A_B = 0.1963 \text{ in}^2$$

$$R_{DS} = 3/8'' \text{ (For \#3 rebar)}$$

Modulus of elasticity of concrete (E_C) = $(\gamma_C)^{1.5} \times (33 \times (f'c)^{0.5})$

$$= (145)^{1.5} \times (33 \times (3500)^{0.5})$$

$$= 3408788 \text{ psi}$$

Modulus of elasticity of steel (E_S) = 29000000 psi

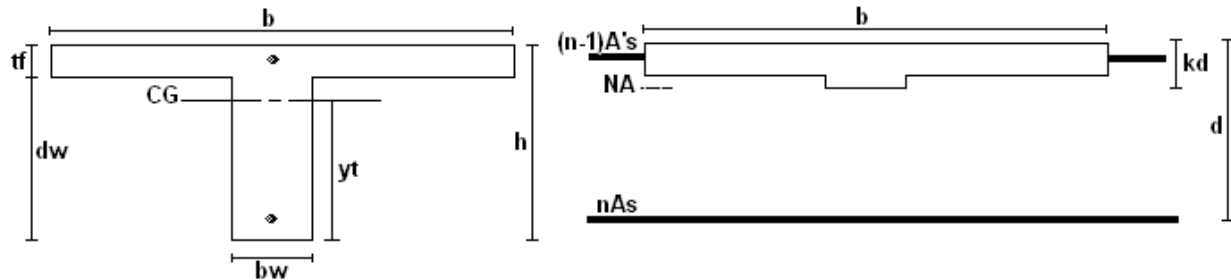
Modular ratio (n) = E_S / E_C

$$= 29000000 / 3408788$$

$$= 8.51$$

Modulus of rupture of concrete (f_r) = $7.5 \times (f'c)^{0.5}$

$$\begin{aligned}
 &= 7.5 \times (3500)^{0.5} \\
 &= 443.7 \text{ psi} \\
 \text{Cracking Moment (M}_{CR}) &= f_r \times I_g / y_t \\
 &= 443.7 \times 1632.1 / 8.1549 \\
 &= 88800.9 \text{ in-lb.}
 \end{aligned}$$



Gross Section

Cracked Transformed Section

$$\begin{aligned}
 y_t &= 8.1549'' \quad (\text{As Provided by Amvic}) \\
 I_g &= 1632.1 \text{ in}^4 \quad (\text{As Provided by Amvic}) \\
 C &= b_{wa} / (n \times A_{S \text{ Pos provided}}) \\
 &= 5.2 / (8.51 \times 0.1963) \\
 &= 3.1128 \\
 f &= t_f \times (b - b_{wa}) / (n \times A_{S \text{ Pos provided}}) \\
 &= 2 \times (32 - 5.2) / (8.51 \times 0.1963) \\
 &= 32.085 \\
 r &= (n-1) A_{S \text{ Neg provided}} / (n A_{S \text{ Pos provided}}) = 0 \quad (\text{As } A_{S \text{ Neg provided}} = 0) \\
 kd &= \frac{\sqrt{C(2d + t_f \times f + 2rd') + (f + r + 1)^2} - (f + r + 1)}{C} \\
 &= \frac{[\{3.1128 \times (2 \times 10.75 + 2 \times 32.085 + 0) + (32.085 + 0 + 1)^2\}^{0.5} - (32.085 + 0 + 1)]}{3.1128} \\
 &= 1.2242
 \end{aligned}$$

Moment of inertia of cracked section transformed to concrete (I_{cr})

$$\begin{aligned}
 &= (b - b_w) t_f^3 / 12 + b_w (kd)^3 / 3 + (b - b_w) t_f (kd - t_f / 2)^2 + n A_{Bi} (d - kd)^2 + (n - 1) A_{Lpi} (kd - d')^2 \\
 &= (32 - 5.2) \times 2^3 / 12 + 5.2 \times (1.2242)^3 / 3 + (32 - 5.2) (2) (1.2242 - 2/2)^2 + 8.51 \times (0.1963) (10.75 - 1.2242)^2 + (10.51 - 1) \times 0 \\
 &= 175.3248 \text{ in}^4
 \end{aligned}$$

Service Moment (M_P)

$$\begin{aligned}
 \text{Dead Load moment, M}_D &= 143.46 \times 10^2 / 8 \times 12 \\
 &= 21519 \text{ lb-in} \\
 \text{Live Load moment, M}_L &= 106.67 \times 10^2 / 8 \times 12 \\
 &= 16000 \text{ lb-in} \\
 \text{Total moment, M}_{D+L} &= 21519 + 16000
 \end{aligned}$$

$$\begin{aligned}
 &= 37519 \text{ lb-in} \\
 \text{Sustained Moment, } M_{\text{SUS}} &= M_D + 0.5 \times M_L \quad (\text{Assume that } 50\% \text{ Load as sustained}) \\
 &= 21519 + 0.5 \times 16000 \\
 &= 29519 \text{ lb-in}
 \end{aligned}$$

Effective moment of inertia for deflection computation (I_e)

A. Under Dead Load

$$\begin{aligned}
 M_{cr} / M_D &= 88800.9 / 21519 \\
 &= 4.1266 \\
 \text{Hence } (I_e)_d &= I_g
 \end{aligned}$$

B. Under Sustained Load

$$\begin{aligned}
 M_{cr} / M_{\text{SUS}} &= 88800.9 / 29519 \\
 &= 3.008 \\
 \text{Hence } (I_e)_d &= I_g
 \end{aligned}$$

C. Under Dead + Live Load

$$\begin{aligned}
 M_{cr} / M_{D+L} &= 88800.9 / 37519 \\
 &= 2.3668 \\
 \text{Hence } (I_e)_d &= I_g
 \end{aligned}$$

8.1.3.3.1 Short Term Deflection

For Continuous beam, the mid-span deflection is $\Delta_i = K (5/48) M_P \times L^2 / (E_c \times I_e)$

Where,

$$\begin{aligned}
 K &= 1.20 - 0.20 M_P / M_O \quad \text{for continuous beam} \\
 &= 0.80 \quad \text{for Continuous fixed-hinged beam, mid span deflection} \\
 &= 0.738 \quad \text{for Continuous fixed-hinged beam, max deflection using} \\
 &\quad \text{maximum moment} \\
 &= 0.60 \quad \text{for fixed-fixed beam} \\
 &= 1.0 \quad \text{for simple span}
 \end{aligned}$$

$$M_O = \text{Simple span moment at mid span, } = (P \times L^2 / 8) \times 12$$

Use $K = 1.0$ to be on conservative side

$$\begin{aligned}
 \Delta_{iD} &= K (5/48) M_D \times L^2 / (E_c \times I_e) \\
 &= 1.0 \times (5/48) \times 21519 \times (10 \times 12)^2 / (3408788 \times 1632.1) \\
 &= \mathbf{0.00580''}
 \end{aligned}$$

$$\begin{aligned}
 \Delta_{iLL} &= K (5/48) M_{LL} \times L^2 / (E_c \times I_e) \\
 &= 1.0 \times (5/48) \times 16000 \times (10 \times 12)^2 / (3408788 \times 1632.1) \\
 &= \mathbf{0.00431''}
 \end{aligned}$$

$$\begin{aligned}
 \Delta_{iSUS} &= K (5/48) M_{\text{SUS}} \times L^2 / (E_c \times I_e) \\
 &= 1.0 \times (5/48) \times 29519 \times (10 \times 12)^2 / (3408788 \times 1632.1)
 \end{aligned}$$

$$= 0.007959''$$

Allowable Deflections

$$\begin{aligned} \Delta_{i \text{ Allow LL}} &= (L \times 12) / \Delta_{\text{Factor Total}} \\ &= (10 \times 12) / 180 \\ &= \mathbf{0.6666''} \\ &> \Delta_{i \text{ LL}} = \mathbf{0.00431''} \text{ (OK)} \end{aligned}$$

8.1.3.3.2 Long term Deflection

i. Sustained load duration of 5 years & more

$$\begin{aligned} \lambda &= \xi / (1 + 50 \times p') \\ &= 2.0 / (1 + 0) \\ &= 2.0 \\ \Delta_{(CP+SH)} &= \lambda \times \Delta_{i \text{ SUS}} \\ &= 2 \times 0.007959 \\ &= 0.015918 \text{ in} \\ \Delta_{(CP+SH)} + \Delta_{i \text{ LL}} &= 0.015918 + 0.00431 \\ &= 0.020228 \text{ in} \end{aligned}$$

Allowable Deflections

$$\begin{aligned} \Delta_{i \text{ Allow}} &= (L \times 12) / \Delta_{\text{Factor}} \\ &= (10 \times 12) / 240 \\ &= \mathbf{0.5''} \\ &> \mathbf{0.020228''} \text{ (OK)} \end{aligned}$$

ii. Sustained load duration of 3 Months

$$\begin{aligned} \text{Sustained Moment, } M_{\text{SUS}} &= M_D + 0.5 \times M_L \quad (\text{Assume that 50\% Load as sustained}) \\ &= 21519 + 0.5 \times 16000 \\ &= 29519 \text{ lb-in} \end{aligned}$$

Under Sustained Load

$$\begin{aligned} M_{cr} / M_{\text{SUS}} &= 88800.9 / 29519 \\ &= 3.008 \\ \text{Hence } (I_e)_{\text{SUS}} &= I_g \\ \Delta_{i \text{ SUS}} &= K (5/48) M_{\text{SUS}} \times L^2 / (E_c \times I_e) \\ &= 1.0 \times (5/48) \times 29519 \times (10 \times 12)^2 / (3408788 \times 1632.1) \\ &= \mathbf{0.000132''} \\ \lambda &= \xi / (1 + 50 \times p') \\ &= 1.0 / (1 + 0) \end{aligned}$$

$$\begin{aligned}
 &= 1.0 \\
 \Delta_{(CP+SH)} &= \lambda \times \Delta_{i\text{SUS}} \\
 &= 1 \times 0.000132 \\
 &= 0.000132 \text{ in} \\
 \Delta_{(CP+SH)} + \Delta_{i\text{LL}} &= 0.000132 + 0.00431 \\
 &= 0.0044 \text{ in}
 \end{aligned}$$

Allowable Deflections

$$\begin{aligned}
 \Delta_{i\text{Allow}} &= (L \times 12) / \Delta_{\text{Factor}} \\
 &= (10 \times 12) / 240 \\
 &= 0.5'' \\
 &> 0.0044'' \text{ (OK)}
 \end{aligned}$$

8.1.4 Calculation for Transverse Slab Reinforcement

Consider 12" width of slab,

$$L_{\text{Slab}} = 27.5 / 12$$

$$= 2.292 \text{ ft}$$

$$\text{Self weight of deck} = 116.794 \text{ (As calculated above)}$$

$$\text{Total factored load, } P_U = 1.2 \times 10 \times 12 / 12 + 1.2 \times 116.794 + 1.6 \times 40 \times 12 / 12$$

$$= 216.15 \text{ plf}$$

$$\text{Maximum Moment} = 216.15 \times 2.29^2 / 12$$

$$= 94.4 \text{ ft-lb}$$

$$= 1133.5 \text{ in-lb}$$

$$\text{Tension controlled reinforcement ratio } (\rho_t) = 0.319 \times 0.85 \times 3500 / 60000$$

$$= 0.0158$$

$$\text{Maximum allowed reinforcement ratio } (\rho_{\text{Max}}) = \rho_t$$

$$= 0.0158$$

$$\text{Minimum reinforcement ratio } (\rho_{\text{Min}}) = \text{Max } (3 \times (f'c)^{0.5}, 200) / f_y$$

$$= \text{Max } (3 \times (3500)^{0.5}, 200) / 60000$$

$$= \text{Max } (177.5, 200) / 60000$$

$$= 200 / 60000$$

$$= 0.0033$$

Reinforcement ratio for +ive moment (ρ_{Pos})

$$= (0.85 \times f'_c / f_y) \times \{1 - [1 - 2 \times M_{UP} / (\phi \times b_w \times t_f / 2^2 \times 0.85 \times f'_c)]^{0.5}\}$$

$$= 1.78 \times 10^{-3}$$

$$= 0.00178 < (\rho_{Min} = 0.0033)$$

$$= 0.00178 < (\rho_{Max} = 0.0158) \text{ OK}$$

$$\text{Area of Reinforcement Required} = 0.00178 \times 12 \times 2/2$$

$$= 0.021 \text{ in}^2$$

Rebar Used = #4 rebar

$$\text{Area of Rebar} = 0.1963 \text{ in}^2$$

$$\text{Spacing} = (0.1963 / 0.021) \times 12$$

$$= 112.71 \text{ in}$$

Per Section 7.12 of ACI-318-02 Spacing of rebar will be Minimum of the following three

- (1) Calculated spacing as above = 112.71 in
- (2) 5 times of thickness of slab = $5 \times 2 = 10$ in
- (3) 18 in

Provide #4 rebar @ 10" O.C.

8.1.5 Calculation for Longitudinal Slab Reinforcement

Consider 12" width of slab,

$$\text{Per Section 7.12 of ACI-318-02 Minimum reinforcement} = 0.0018 \times \text{area of cross section}$$

$$= 0.0018 \times 2 \times 12$$

$$= 0.0432 \text{ in}$$

$$\text{Spacing} = (0.1963 / 0.0432) \times 12$$

$$= 54.52 \text{ in}$$

Per Section 7.12 of ACI-318-02 Spacing of rebar will be Minimum of the following three

- (1) Calculated spacing as above = 54.52 in
- (2) 5 times of thickness of slab = $5 \times 2 = 10$ in
- (3) 18 in

Provide #4 rebar @ 10" O.C.

8.2 Double Span Joist

(12" Panel Size With 10" Deep Joist @ 32" O.C. And 2" Topping Slab)

8.2.6 Inputs

Panel Designation	=	12" Panel section with 10" deep beam
Beam Depth (dw)	=	10"
Topping (t _f)	=	2"
Minimum Beam Width, bottom (b _w)	=	6.5"
Average Joist Width (b _{wa})	=	5.2"
Panel Span, Transverse (b)	=	32"
Maximum Span of the Deck (L)	=	10'-0"
Number of Span	=	Double
Live load acting on the deck (w _{LL})	=	40 psf
Dead load acting on the deck (w _{DL})	=	10 psf
Unit weight of concrete (γ _c)	=	145 pcf
Specified compressive strength of concrete (f' _c)	=	3500 psi
Yield strength of rebar (f _y)	=	60000 psi
Rebar cover, Center of rebar (c)	=	1.25"
Allowable Deflection factor, Total (Δ _{Factor LL})	=	360 (Short Term)
Allowable Deflection factor, Total (Δ _{Factor LL})	=	480 (Long Term)

8.2.7 Analysis

Dead Load factor (K _{DL})	=	1.2
Live Load factor (K _{LL})	=	1.6

Section Properties

Cross-section area A	=	115.9888 in ² (Refer Table on Page – 7)
Distance of CG from top (CG _{Top})	=	3.8451 in from top
Moment of inertia about x-axis (I _{xx})	=	1632.1 in ⁴
Section Modulus about x-axis (S _{xx})	=	1632.1 / {Max [3.8451, (10 + 2 – 3.8451)]}
	=	200.137 in ³
Effective depth (d)	=	d _w – c + t _f
	=	10 – 1.25 + 2
	=	10.75"
Self weight of deck (w _{Self})	=	w _C x A _{Gross}
	=	145 x 115.9888/144
	=	116.794 plf
Total Dead Load W _{DTotal}	=	Self Weight + Applied Additional Dead Load
	=	116.794 + 10 x 32/12
	=	143.46 plf

$$\begin{aligned}
 \text{Live Load } W_{LL} &= 40 \times 32/12 \\
 &= 106.67 \text{ plf} \\
 \text{Total Un-factored Load } W_P &= W_{D \text{ Total}} + W_{LL} \\
 &= 143.46 + 106.67 \\
 &= 250.13 \text{ plf} \\
 \text{Total factored load } (P_U) &= \{K_{DL} \times W_{D \text{ Total}} + K_{LL} \times W_{LL}\} \\
 &= 1.2 \times 143.46 + 1.6 \times 106.67 \\
 &= 342.824 \text{ plf} \\
 \text{Maximum Shear Force } (V_U) &= P_U \times L / 2 \\
 &= 342.824 \times 10 / 2 \\
 &= 1714.12 \text{ lb.} \\
 \text{Maximum Positive Moment } (M_{UP}) &= (P_U \times L^2 / 14) \times 12 \\
 &= (342.824 \times 10^2 / 14) \times 12 \\
 &= 29384.91 \text{ in-lb.} \\
 \text{Maximum Negative Moment } (M_{UN}) &= (P_U \times L^2 / 16) \times 12 \text{ \{At Exterior Support of Double Span\}} \\
 &= (342.824 \times 10^2 / 16) \times 12 = 25711.8 \text{ in-lb.} \\
 &= (P_U \times L^2 / 9) \times 12 \text{ \{At 1st Interior Support of Double Span\}} \\
 &= (342.824 \times 10^2 / 9) \times 12 = 45709.87 \text{ in-lb.}
 \end{aligned}$$

8.2.8 Design

8.2.8.1 Shear Strength

$$\begin{aligned}
 \text{Shear Strength of the section } (\phi V_c) &= 1.1 \times 0.75 \times 2 \times (f'c)^{0.5} \times b_{wa} \times d \\
 &= 1.1 \times 0.75 \times 2 \times (3500)^{0.5} \times 5.2 \times 10.75 \\
 &= \mathbf{5456.69 \text{ lb.} > V_U (= 1714.12 \text{ lb.})} \quad \text{(OK)}
 \end{aligned}$$

8.2.8.2 Moment Strength

$$\begin{aligned}
 \text{Strength reduction factor } (\phi) &= 0.9 \\
 \beta_1 &= 0.85 \quad \text{if } (f'c \leq 4000 \text{ psi}) \\
 \text{Tension controlled reinforcement ratio } (\rho_b) &= 0.319 \times 0.85 \times 3500 / 60000 \\
 &= 0.0158 \\
 \text{Maximum allowed reinforcement ratio } (\rho_{Max}) &= \rho_t \\
 &= 0.0158 \\
 \text{Minimum reinforcement ratio } (\rho_{Min}) &= \text{Max } (3 \times (f'c)^{0.5}, 200) / f_y \\
 &= \text{Max } (3 \times (3500)^{0.5}, 200) / 60000 \\
 &= \text{Max } (177.5, 200) / 60000 \\
 &= 200 / 60000 \\
 &= 0.0033
 \end{aligned}$$

Positive Reinforcement

Reinforcement ratio for +ive moment (ρ_{Pos})

$$\begin{aligned}
 &= (0.85 \times f'c / fy) \times \{1 - [1 - 2 \times M_{UP} / (\phi \times b_{wa} \times d^2 \times 0.85 \times f'c)]^{0.5}\} \\
 &= (0.85 \times 3500/60000) \{1 - [1 - 2 \times 29384.9 / (0.9 \times 5.2 \times 10.75^2 \times 0.85 \times 3500)]^{0.5}\} \\
 &= 0.0009139 < (\rho_{Min} = 0.0033) \\
 &= 0.0033 < (\rho_{Max} = 0.0158) \quad \mathbf{OK}
 \end{aligned}$$

Area of reinforcement required ($A_{S_{Pos}} req$) = $\rho_{Pos} \times b_{wa} \times d$

$$\begin{aligned}
 &= 0.0033 \times 5.2 \times 10.75 \\
 &= 0.18477 \text{ in}^2
 \end{aligned}$$

$A_{S_{Pos}}$ provided = 1 # 4 (Area = 0.1963 in² > 0.18447) **OK**

Negative Reinforcement

Reinforcement ratio for -ive moment (ρ_{Neg})

$$\begin{aligned}
 &= (0.85 \times f'c / fy) \times \{1 - [1 - 2 \times M_{UN} / (\phi \times b_{wa} \times d^2 \times 0.85 \times f'c)]^{0.5}\} \\
 &= (0.85 \times 3500/60000) \{1 - [1 - 2 \times 45709.8 / (0.9 \times 5.2 \times 10.75^2 \times 0.85 \times 3500)]^{0.5}\} \\
 &= 0.001429 < (\rho_{Min} = 0.0033) \\
 &= 0.0033 < (\rho_{Max} = 0.0158) \quad \mathbf{OK}
 \end{aligned}$$

Area of reinforcement required ($A_{S_{Neg}} req$) = $\rho_{Neg} \times b_{wa} \times d$

$$\begin{aligned}
 &= 0.0033 \times 5.2 \times 10.75 \\
 &= 0.18447 \text{ in}^2
 \end{aligned}$$

$A_{S_{Neg}}$ provided = 1 # 4 (Area = 0.1963 in² > 0.18447) **OK**

Nominal moment strength

Plain Concrete

Nominal moment strength of the section (ϕMn) = $0.65 \times 5 (f'c)^{0.5} \times S_{XX}$

$$\begin{aligned}
 &= 0.65 \times 5 \times (3500)^{0.5} \times 200.137 \\
 &= 38480.8594 \text{ in-lb.}
 \end{aligned}$$

Reinforced Concrete

Nominal moment strength of the section (ϕMn)

$$\begin{aligned}
 &= \phi A_{S_{Pos}} \text{ provided} \times fy \times [d - (A_{S_{Pos}} \text{ provided} \times fy / (0.85 \times f'c \times b))/2] \\
 &= 0.9 \times 0.1963 \times 60000 \times [10.75 - (0.1963 \times 60000 / (0.85 \times 3500 \times 32))/2] \\
 &= 113296.43 \text{ in-lb.}
 \end{aligned}$$

8.2.8.3 Deflection

Total depth of section (h) = $d_w + t_f = 10 + 2 = 12''$

$A_{LP} = A_{S_{Neg}} \text{ provided} = 0.1963 \text{ in}^2$

$A_B = A_{S_{Pos}} \text{ provided} = 0.1963 \text{ in}^2$

$R_{DS} = \text{Diameter of shear rebar} = 3/8''$ (For #3 rebar)

$R_{DLP} = \text{Diameter of Single rebar } A_{S_{Neg}} \text{ provided} = 0.5''$ (For #4 rebar)

Effective depth (d_{LP}) = $d_w + t_f - c - R_{DS} - 0.5R_{DLP}$

$$\begin{aligned}
 &= 10 + 2 - 1.25 - 3/8 - 0.5 (0.5)
 \end{aligned}$$

= 10.125"

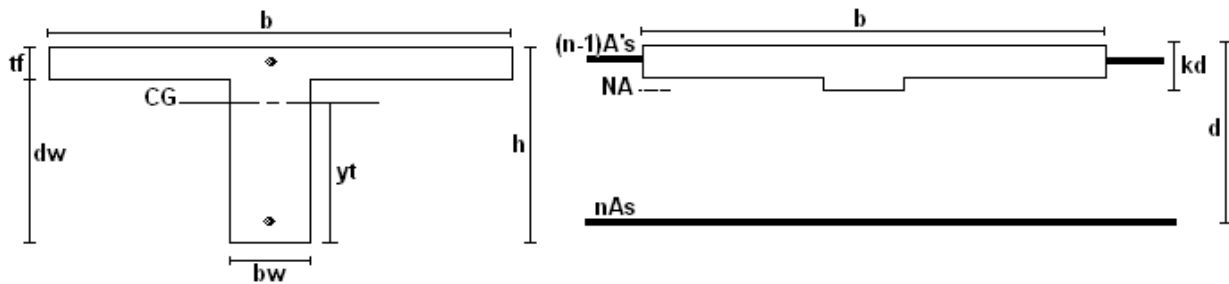
Modulus of elasticity of concrete (E_C) = $(\gamma_C)^{1.5} \times (33 \times (f'_c)^{0.5})$
 = $(145)^{1.5} \times (33 \times (3500)^{0.5})$
 = 3408788 psi

Modulus of elasticity of steel (E_S) = 29000000 psi

Modular ratio (n) = E_S / E_C
 = $29000000 / 3408788$
 = 8.51

Modulus of rupture of concrete (f_r) = $7.5 \times (f'_c)^{0.5}$
 = $7.5 \times (3500)^{0.5}$
 = 443.7 psi

Cracking Moment (M_{CR}) = $f_r \times I_g / y_t$
 = $443.7 \times 1632.1 / 8.1549$
 = 88800.9 in-lb.



Gross Section

Cracked Transformed Section

y_t = 8.1549" (As Provided by Amvic)

I_g = 1632.1 in⁴ (As Provided by Amvic)

C = $b_{wa} / (n \times A_{S \text{ Pos provided}})$
 = $5.2 / (8.51 \times 0.1963)$
 = 3.1128

f = $t_f \times (b - b_{wa}) / (n \times A_{S \text{ Pos provided}})$
 = $2 \times (32 - 5.2) / (8.51 \times 0.1963)$
 = 32.085

r = $(n-1) A_{S \text{ Neg provided}} / (n A_{S \text{ Pos provided}})$
 = $(8.51-1) \times (0.1963) / (8.51 \times 0.1963)$
 = 0.8825

d' = $h - d_{LP} = 12 - 10.125 = 1.875"$

kd = $\frac{\sqrt{C(2d + t_f \times f + 2rd')} + (f + r + 1)^2 - (f + r + 1)}{C}$

$$= \frac{[(3.1128 \times (2 \times 10.75 + 2 \times 32.085 + 2 \times 0.8825 \times 1.875) + (32.085 + 0.8825 + 1)^2]^{0.5} - (32.085 + 0.8825 + 1)}{3.1128}$$

$$= 1.2393$$

Moment of inertia of cracked section transformed to concrete (I_{cr})

$$= (b - b_w) t_f^3 / 12 + b_w (kd)^3 / 3 + (b - b_w) t_f (kd - t_f / 2)^2 + n A_{Bi} (d - kd)^2 + (n - 1) A_{Lpi} (kd - d')^2$$

$$= (32 - 5.2) \times 2^3 / 12 + 5.2 \times (1.2393)^3 / 3 + (32 - 5.2) (2) (1.2393 - 2/2)^2 + 8.51 \times (0.1963) (10.75 - 1.2393)^2 + (8.51 - 1) \times 0.1963 \times (1.2393 - 1.875)^2$$

$$= 209.43 \text{ in}^4$$

Dead Load moment, M_D = $143.46 \times 10^2 / 14 \times 12$
= 12296.57 lb-in

Live Load moment, M_L = $106.67 \times 10^2 / 14 \times 12$
= 9142.86 lb-in

Total moment, M_{D+L} = $12296.57 + 9142.86$
= 21439.43 lb-in

Sustained Moment, M_{SUS} = $M_D + 0.5 \times M_L$ (Assume that 50% Load as sustained)
= $12296.57 + 0.5 \times 9142.86$
= 16868.0 lb-in

Effective moment of inertia for deflection computation (I_e)

A. Under Dead Load

$$M_{cr} / M_D = 88800.9 / 12296.57$$

$$= 7.221$$

Hence $(I_e)_d = I_g$

B. Under Sustained Load

$$M_{cr} / M_{SUS} = 88800.9 / 16868.0$$

$$= 5.264$$

Hence $(I_e)_d = I_g$

C. Under Dead + Live Load

$$M_{cr} / M_{D+L} = 88800.9 / 21439.43$$

$$= 4.142$$

Hence $(I_e)_d = I_g$

8.2.8.3.1 Short Term Deflection

For Continuous beam, the mid-span deflection is $\Delta_i = K (5/48) M_P \times L^2 / (E_c \times I_e)$

Where,

$$\begin{aligned}
 K &= 1.20 - 0.20 M_P / M_O \quad \text{for continuous beam} \\
 &= 0.80 \quad \text{for Continuous fixed-hinged beam, mid span deflection} \\
 &= 0.738 \quad \text{for Continuous fixed-hinged beam, max deflection using} \\
 &\quad \text{maximum moment} \\
 &= 0.60 \quad \text{for fixed-fixed beam} \\
 &= 1.0 \quad \text{for simple span}
 \end{aligned}$$

$$M_O = \text{Simple span moment at mid span,} = (P \times L^2 / 8) \times 12$$

Use $K = 1.0$ to be on conservative side

$$\begin{aligned}
 \Delta_{iD} &= K (5/48) M_D \times L^2 / (E_c \times I_e) \\
 &= 1 \times (5/48) \times 12296.57 \times (10 \times 12)^2 / (3408788 \times 1632.1) \\
 &= \mathbf{0.00331''}
 \end{aligned}$$

$$\begin{aligned}
 \Delta_{iLL} &= K (5/48) M_{LL} \times L^2 / (E_c \times I_e) \\
 &= 1 \times (5/48) \times 9142.86 \times (10 \times 12)^2 / (3408788 \times 1632.1) \\
 &= \mathbf{0.002465''}
 \end{aligned}$$

$$\begin{aligned}
 \Delta_{iSUS} &= K (5/48) M_{SUS} \times L^2 / (E_c \times I_e) \\
 &= 1 \times (5/48) \times 16868.0 \times (10 \times 12)^2 / (3408788 \times 1632.1) \\
 &= \mathbf{0.004548''}
 \end{aligned}$$

Allowable Deflections

$$\begin{aligned}
 \Delta_{i \text{ Allow LL}} &= (L \times 12) / \Delta_{\text{Factor Total}} \\
 &= (10 \times 12) / 180 \\
 &= \mathbf{0.6666''} \\
 &> \Delta_{iLL} = \mathbf{0.002465''} \text{ (OK)}
 \end{aligned}$$

8.2.8.3.2 Long term Deflection

$$p' = 0.1963 / (5.2 \times 10.75) = 0.0035$$

i. Sustained load duration of 5 years & more

$$\begin{aligned}
 \lambda &= \xi / (1 + 50 \times p') \\
 &= 2.0 / (1 + 50 \times 0.0035) \\
 &= \mathbf{1.702}
 \end{aligned}$$

$$\begin{aligned}
 \Delta_{(CP+SH)} &= \lambda \times \Delta_{iSUS} \\
 &= \mathbf{1.702 \times 0.004548} \\
 &= \mathbf{0.007741 \text{ in}}
 \end{aligned}$$

$$\begin{aligned}
 \Delta_{(CP+SH)} + \Delta_{iLL} &= \mathbf{0.007741 + 0.002465} \\
 &= \mathbf{0.0102 \text{ in}}
 \end{aligned}$$

Allowable Deflections

$$\begin{aligned} \Delta_{i \text{ Allow}} &= (L \times 12) / \Delta_{\text{Factor}} \\ &= (10 \times 12) / 240 \\ &= \mathbf{0.5''} \\ &> \mathbf{0.0102'' \text{ (OK)}} \end{aligned}$$

ii. Sustained load duration of 3 Months

$$\begin{aligned} \text{Sustained Moment, } M_{\text{SUS}} &= M_D + 0.5 \times M_L \quad (\text{Assume that 50\% Load as sustained}) \\ &= 12296.57 + 0.5 \times 9142.86 \\ &= 16868 \text{ lb-in} \end{aligned}$$

Under Sustained Load

$$\begin{aligned} M_{\text{cr}} / M_{\text{SUS}} &= 88800.9 / 16868 \\ &= 5.264 \end{aligned}$$

$$\text{Hence } (I_e)_d = I_g$$

$$\begin{aligned} \Delta_{i \text{ SUS}} &= K (5/48) M_{\text{SUS}} \times L^2 / (E_c \times I_e) \\ &= 1.0 \times (5/48) \times 16868 \times (10 \times 12)^2 / (3408788 \times 1632.1) \\ &= \mathbf{0.004548''} \end{aligned}$$

$$\begin{aligned} \lambda &= \xi / (1 + 50 \times p') \\ &= 1.0 / (1 + 50 \times 0.0035) \\ &= \mathbf{0.851} \end{aligned}$$

$$\begin{aligned} \Delta_{(\text{CP+SH})} &= \lambda \times \Delta_{i \text{ SUS}} \\ &= \mathbf{0.851 \times 0.004548} \\ &= \mathbf{0.00387 \text{ in}} \end{aligned}$$

$$\begin{aligned} \Delta_{(\text{CP+SH})} + \Delta_{i \text{ LL}} &= \mathbf{0.00387 + 0.002465} \\ &= \mathbf{0.00634 \text{ in}} \end{aligned}$$

Allowable Deflections

$$\begin{aligned} \Delta_{i \text{ Allow}} &= (L \times 12) / \Delta_{\text{Factor}} \\ &= (10 \times 12) / 240 \\ &= \mathbf{0.5''} \\ &> \mathbf{0.00634'' \text{ (OK)}} \end{aligned}$$

8.2.9 Calculation for Transverse Slab Reinforcement

Consider 12" width of slab,

$$L_{\text{Slab}} = 27.5 / 12$$

$$= 2.292 \text{ ft}$$

$$\text{Self weight of deck} = 116.794 \text{ (As calculated above)}$$

$$\text{Total factored load, } P_U = 1.2 \times 10 \times 12 / 12 + 1.2 \times 116.794 + 1.6 \times 40 \times 12 / 12$$

$$= 216.15 \text{ plf}$$

$$\text{Maximum Moment} = 216.15 \times 2.29^2 / 12$$

$$= 94.4 \text{ ft-lb}$$

$$= 1133.5 \text{ in-lb}$$

$$\text{Tension controlled reinforcement ratio } (\rho_t) = 0.319 \times 0.85 \times 3500 / 60000$$

$$= 0.0158$$

$$\text{Maximum allowed reinforcement ratio } (\rho_{\text{Max}}) = \rho_t$$

$$= 0.0158$$

$$\text{Minimum reinforcement ratio } (\rho_{\text{Min}}) = \text{Max } (3 \times (f'c)^{0.5}, 200) / f_y$$

$$= \text{Max } (3 \times (3500)^{0.5}, 200) / 60000$$

$$= \text{Max } (177.5, 200) / 60000$$

$$= 200 / 60000$$

$$= 0.0033$$

Consulting Engineers, Corp

Project: AmDeck Design Guide
Client: Amvic, Inc.

Prepared by: Kapil
Checked by: Andy / Raj

Date: 05/01/2007
Date: 05/01/2007

Reinforcement ratio for +ive moment (ρ_{Pos})

$$\begin{aligned} &= (0.85 \times f'_c / f_y) \times \{1 - [1 - 2 \times M_{UP} / (\phi \times b_w \times t_f / 2^2 \times 0.85 \times f'_c)]^{0.5}\} \\ &= 1.78 \times 10^{-3} \\ &= 0.00178 < (\rho_{Min} = 0.0033) \\ &= 0.00178 < (\rho_{Max} = 0.0158) \text{ OK} \end{aligned}$$

$$\begin{aligned} \text{Area of Reinforcement Required} &= 0.00178 \times 12 \times 2/2 \\ &= 0.021 \text{ in}^2 \end{aligned}$$

Rebar Used = #4 rebar

Area of Rebar = 0.1963 in²

Spacing = (0.1963 / 0.021) x 12
= 112.71 in

Per Section 7.12 of ACI-318-02 Spacing of rebar will be Minimum of the following three

- (1) Calculated spacing as above = 112.71 in
- (2) 5 times of thickness of slab = 5 x 2 = 10 in
- (3) 18 in

Provide #4 rebar @ 10" O.C.

8.2.10 Calculation for Longitudinal Slab Reinforcement

Consider 12" width of slab,

$$\begin{aligned} \text{Per Section 7.12 of ACI-318-02 Minimum reinforcement} &= 0.0018 \times \text{area of cross section} \\ &= 0.0018 \times 2 \times 12 \\ &= 0.0432 \text{ in} \end{aligned}$$

Spacing = (0.1963 / 0.0432) x 12
= 54.52 in

Per Section 7.12 of ACI-318-02 Spacing of rebar will be Minimum of the following three

- (1) Calculated spacing as above = 54.52 in
- (2) 5 times of thickness of slab = 5 x 2 = 10 in
- (3) 18 in

Provide #4 rebar @ 10" O.C.

8.3 Multiple Span Joist

(12" Panel Size With 10" Deep Joist @ 32" O.C. And 2" Topping Slab)

Inputs

Panel Designation	=	12" Panel section with 10" deep beam
Beam Depth (dw)	=	10"
Topping (ti)	=	2"
Minimum Beam Width, bottom (bw)	=	6.5"
Average Joist Width (bwa)	=	5.2"
Panel Span, Transverse (b)	=	32"
Maximum Span of the Deck (L)	=	10'-0"
Number of Span	=	Multiple
Live load acting on the deck (wLL)	=	40 psf
Dead load acting on the deck (wDL)	=	10 psf
Unit weight of concrete (γc)	=	145 pcf
Specified compressive strength of concrete (f'c)	=	3500 psi
Yield strength of rebar (fy)	=	60000 psi
Rebar cover, Center of rebar (c)	=	1.25"
Allowable Deflection factor, Total (ΔFactor LL)	=	360 (Short Term)
Allowable Deflection factor, Total (ΔFactor LL)	=	480 (Long Term)

8.3.1 Analysis

Dead Load factor (K _{DL})	=	1.2
Live Load factor (K _{LL})	=	1.6

Section Properties

Cross-section area A	=	115.9888 in ²	(Refer Table on Page – 7)
Distance of CG from top (CG _{Top})	=	3.8451 in	from top
Moment of inertia about x-axis (I _{xx})	=	1632.1 in ⁴	
Section Modulus about x-axis (S _{xx})	=	1632.1 / {Max [3.8451, (10 + 2 – 3.8451)]}	
	=	200.137 in ³	
Effective depth (d)	=	d _w – c + t _i	
	=	10 – 1.25 + 2	= 10.75"
Self weight of deck (w _{Self})	=	w _C × A _{Gross}	
	=	145 × 115.9888/144	= 116.794 plf
Total Dead Load W _{DTotal}	=	Self Weight + Applied Additional Dead Load	
	=	116.794 + 10 × 32/12	= 143.46 plf
Live Load W _{LL}	=	40 × 32/12	= 106.67 plf
Total un-factored Load W _P	=	W _{D Total} + W _{LL}	
	=	143.46 + 106.67	= 250.13 plf

$$\begin{aligned}
 \text{Total factored load (P}_U\text{)} &= \{K_{DL} \times W_{D \text{ Total}} + K_{LL} \times W_{LL}\} \\
 &= 1.2 \times 143.46 + 1.6 \times 106.67 = 342.824 \text{ plf} \\
 \text{Maximum Shear Force (V}_U\text{)} &= 1.15 \times P_U \times L / 2 \text{ \{For Multiple Span\}} \\
 &= 1.15 \times 342.824 \times 10 / 2 \\
 &= 1971.24 \text{ lb.} \\
 \text{Maximum Positive Moment (M}_{UP}\text{)} & \\
 &= (P_U \times L^2 / 14) \times 12 \quad \text{\{At End Spans of Multiple Span\}} \\
 &= (342.824 \times 10^2 / 14) \times 12 = 29384.91 \text{ in-lb.} \\
 &= (P_U \times L^2 / 16) \times 12 \text{ \{At Interior Spans of Multiple Span\}} \\
 &= (342.824 \times 10^2 / 16) \times 12 = 25711.8 \text{ in-lb.} \\
 \text{Maximum Negative Moment (M}_{UN}\text{)} & \\
 &= (P_U \times L^2 / 16) \times 12 \quad \text{\{At Exterior Support of Multiple Span\}} \\
 &= (342.824 \times 10^2 / 16) \times 12 = 25711.8 \text{ in-lb.} \\
 &= (P_U \times L^2 / 10) \times 12 \quad \text{\{At 1}^{st}\text{ Interior Support of Multiple Span\}} \\
 &= (342.824 \times 10^2 / 10) \times 12 = 41138.88 \text{ in-lb.} \\
 &= (P_U \times L^2 / 11) \times 12 \text{ \{At Other Interior Support of Multiple Span\}} \\
 &= (342.824 \times 10^2 / 11) \times 12 = 37398.98 \text{ in-lb.}
 \end{aligned}$$

8.3.2 Design

8.3.2.1 Shear Strength

$$\begin{aligned}
 \text{Shear Strength of the section } (\phi V_c) &= 1.1 \times 0.75 \times 2 \times (f'_c)^{0.5} \times b_{wa} \times d \\
 &= 1.1 \times 0.75 \times 2 \times (3500)^{0.5} \times 5.2 \times 10.75 \\
 &= \mathbf{5456.69 \text{ lb.} > V_U (= 1714.12 \text{ lb.})} \quad \text{\textbf{(OK)}}
 \end{aligned}$$

8.3.2.2 Moment Strength

$$\begin{aligned}
 \text{Strength reduction factor } (\phi) &= 0.9 \\
 \beta_1 &= 0.85 \quad \text{if } (f'_c \leq 4000 \text{ psi}) \\
 \text{Tension controlled reinforcement ratio } (\rho_b) &= 0.319 \times 0.85 \times 3500 / 60000 \\
 &= 0.0158 \\
 \text{Maximum allowed reinforcement ratio } (\rho_{Max}) &= \rho_t \\
 &= 0.0158 \\
 \text{Minimum reinforcement ratio } (\rho_{Min}) &= \text{Max } (3 \times (f'_c)^{0.5}, 200) / f_y \\
 &= \text{Max } (3 \times (3500)^{0.5}, 200) / 60000 \\
 &= \text{Max } (177.5, 200) / 60000 \\
 &= 200 / 60000 \\
 &= 0.0033
 \end{aligned}$$

Positive Reinforcement

Reinforcement ratio for +ive moment (ρ_{Pos})

$$= (0.85 \times f'_c / f_y) \times \{1 - [1 - 2 \times M_{UP} / (\phi \times b_{wa} \times d^2 \times 0.85 \times f'_c)]^{0.5}\}$$

$$\begin{aligned}
 &= (0.85 \times 3500/60000) \{1 - [1 - 2 \times 29384.91 / (0.9 \times 5.2 \times 10.75^2 \times 0.85 \times 3500)]^{0.5}\} \\
 &= 0.0009139 < (\rho_{\text{Min}} = 0.0033) \\
 &= 0.0033 < (\rho_{\text{Max}} = 0.0158) \text{ OK}
 \end{aligned}$$

$$\begin{aligned}
 \text{Area of reinforcement required (A}_{S \text{ Pos req}}) &= \rho_{\text{Pos}} \times b_w a \times d \\
 &= 0.0033 \times 5.2 \times 10.75 \\
 &= 0.18477 \text{ in}^2
 \end{aligned}$$

$$A_{S \text{ Pos provided}} = 1 \# 4 \text{ (Area} = 0.1963 \text{ in}^2 > 0.18477) \text{ OK}$$

Negative Reinforcement

Reinforcement ratio for -ive moment (ρ_{Neg})

$$\begin{aligned}
 &= (0.85 \times f'c / fy) \times \{1 - [1 - 2 \times M_{\text{UN}} / (\phi \times b_w a \times d^2 \times 0.85 \times f'c)]^{0.5}\} \\
 &= (0.85 \times 3500/60000) \{1 - [1 - 2 \times 41138.88 / (0.9 \times 5.2 \times 10.75^2 \times 0.85 \times 3500)]^{0.5}\} \\
 &= 0.001284 < (\rho_{\text{Min}} = 0.0033) \\
 &= 0.0033 < (\rho_{\text{Max}} = 0.0158) \text{ OK}
 \end{aligned}$$

$$\begin{aligned}
 \text{Area of reinforcement required (A}_{S \text{ Neg req}}) &= \rho_{\text{Neg}} \times b_w a \times d \\
 &= 0.0033 \times 5.2 \times 10.75 \\
 &= 0.18447 \text{ in}^2
 \end{aligned}$$

$$A_{S \text{ Neg provided}} = 1 \# 4 \text{ (Area} = 0.1963 \text{ in}^2 > 0.18447) \text{ OK}$$

Nominal moment strength

Plain Concrete

$$\begin{aligned}
 \text{Nominal moment strength of the section } (\phi Mn) &= 0.65 \times 5 (f'c)^{0.5} \times S_{XX} \\
 &= 0.65 \times 5 \times (3500)^{0.5} \times 200.137 \\
 &= 38480.8594 \text{ in-lb.}
 \end{aligned}$$

Reinforced Concrete

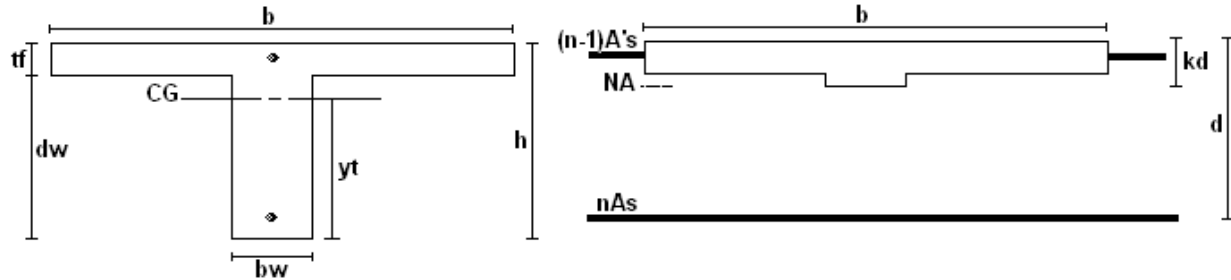
Nominal moment strength of the section (ϕMn)

$$\begin{aligned}
 &= \phi A_{S \text{ Pos provided}} \times fy \times [d - (A_{S \text{ Pos provided}} \times fy / (0.85 \times f'c \times b))/2] \\
 &= 0.9 \times 0.1963 \times 60000 \times [10.75 - (0.1963 \times 60000 / (0.85 \times 3500 \times 32))/2] \\
 &= 113296.43 \text{ in-lb.}
 \end{aligned}$$

8.3.2.3 Deflection

$$\begin{aligned}
 \text{Total depth of section (h)} &= d_w + t_f \\
 &= 10 + 2 \\
 &= 12'' \\
 A_{LP} &= 0 \text{ in}^2 \\
 A_B &= 0.1963 \text{ in}^2 \\
 R_{DS} &= 3/8'' \text{ (For \#3 rebar)} \\
 \text{Modulus of elasticity of concrete (E}_C) &= (\gamma_C)^{1.5} \times (33 \times (f'c)^{0.5})
 \end{aligned}$$

$$\begin{aligned}
 &= (145)^{1.5} \times (33 \times (3500)^{0.5}) \\
 &= 3408788 \text{ psi} \\
 \text{Modulus of elasticity of steel (E}_s\text{)} &= 29000000 \text{ psi} \\
 \text{Modular ratio (n)} &= E_s / E_c \\
 &= 29000000 / 3408788 \\
 &= 8.51 \\
 \text{Modulus of rupture of concrete (f}_r\text{)} &= 7.5 \times (f'_c)^{0.5} \\
 &= 7.5 \times (3500)^{0.5} \\
 &= 443.7 \text{ psi} \\
 \text{Cracking Moment (M}_{CR}\text{)} &= f_r \times I_g / y_t \\
 &= 443.7 \times 1632.1 / 8.1549 \\
 &= 88800.9 \text{ in-lb.}
 \end{aligned}$$



Gross Section

Cracked Transformed Section

$$\begin{aligned}
 y_t &= 8.1549'' \quad (\text{As Provided by Amvic}) \\
 I_g &= 1632.1 \text{ in}^4 \quad (\text{As Provided by Amvic}) \\
 C &= b_{wa} / (n \times A_{S \text{ Pos provided}}) \\
 &= 5.2 / (8.51 \times 0.1963) \\
 &= 3.1128 \\
 f &= t_f \times (b - b_{wa}) / (n \times A_{S \text{ Pos provided}}) \\
 &= 2 \times (32 - 5.2) / (8.51 \times 0.1963) \\
 &= 32.085 \\
 r &= (n-1) A_{S \text{ Neg provided}} / (n A_{S \text{ Pos provided}}) \\
 &= (8.51-1) \times (0.1963) / (8.51 \times 0.1963) \\
 &= 0.8825 \\
 d' &= h - d_{LP} = 12 - 10.125 = 1.875'' \\
 kd &= \frac{\sqrt{C(2d + t_f \times f + 2rd') + (f + r + 1)^2} - (f + r + 1)}{C} \\
 &= \frac{[\{3.1128 \times (2 \times 10.75 + 2 \times 32.085 + 2 \times 0.8825 \times 1.875) + (32.085 + 0.8825 + 1)^2\}^{0.5} - (32.085 + 0.8825 + 1)]}{3.1128} \\
 &= 1.2393
 \end{aligned}$$

Moment of inertia of cracked section transformed to concrete (I_{cr})

$$\begin{aligned}
 &= (b - b_w)t_f^3 / 12 + b_w(kd)^3 / 3 + (b - b_w)t_f(kd - t_f / 2)^2 + nA_{Bi}(d - kd)^2 + (n - 1)A_{Lpi}(kd - d')^2 \\
 &= (32 - 5.2) \times 2^3 / 12 + 5.2 \times (1.2393)^3 / 3 + (32 - 5.2)(2)(1.2393 - 2/2)^2 + 8.51 \times (0.1963)(10.75 - \\
 &\quad 1.2393)^2 + (8.51 - 1) \times 0.1963 \times (1.2393 - 1.875)^2 \\
 &= 209.43 \text{ in}^4
 \end{aligned}$$

Service Moment (M_P)

Dead Load moment, M_D	=	$143.46 \times 10^2 / 14 \times 12$
	=	12296.57 lb-in
Live Load moment, M_L	=	$106.67 \times 10^2 / 14 \times 12$
	=	9142.86 lb-in
Total moment, M_{D+L}	=	12296.57 + 9142.86
	=	21439.43 lb- in
Sustained Moment, M_{SUS}	=	$M_D + 0.5 \times M_L$ (Assume that 50% Load as sustained)
	=	12296.57 + 0.5 x 9142.86
	=	16868.0 lb-in

Effective moment of inertia for deflection computation (I_e)

A. Under Dead Load

$$\begin{aligned}
 M_{cr} / M_D &= 88800.9 / 12296.57 \\
 &= 7.221 \\
 \text{Hence } (I_e)_d &= I_g
 \end{aligned}$$

B. Under Sustained Load

$$\begin{aligned}
 M_{cr} / M_{SUS} &= 88800.9 / 16868.0 \\
 &= 5.264 \\
 \text{Hence } (I_e)_d &= I_g
 \end{aligned}$$

C. Under Dead + Live Load

$$\begin{aligned}
 M_{cr} / M_{D+L} &= 88800.9 / 21439.43 \\
 &= 4.142 \\
 \text{Hence } (I_e)_d &= I_g
 \end{aligned}$$

8.3.2.3.1 Short Term Deflection

For Continuous beam, the mid-span deflection is $\Delta_i = K (5/48) M_P \times L^2 / (E_c \times I_e)$

Where,

$$\begin{aligned}
 K &= 1.20 - 0.20 M_P / M_O \quad \text{for continuous beam} \\
 &= 0.80 \quad \text{for Continuous fixed-hinged beam, mid span deflection}
 \end{aligned}$$

$$\begin{aligned}
 &= 0.738 \quad \text{for Continuous fixed-hinged beam, max deflection using} \\
 &\quad \text{maximum moment} \\
 &= 0.60 \quad \text{for fixed-fixed beam} \\
 &= 1.0 \quad \text{for simple span}
 \end{aligned}$$

M_O = Simple span moment at mid span, = $(P \times L^2 / 8) \times 12$

$$\begin{aligned}
 \Delta_{iD} &= K (5/48) M_D \times L^2 / (E_c \times I_e) \\
 &= 0.8 \times (5/48) \times 12296.57 \times (10 \times 12)^2 / (3408788 \times 1632.1) \\
 &= \mathbf{0.002652''} \\
 \Delta_{iLL} &= K (5/48) M_{LL} \times L^2 / (E_c \times I_e) \\
 &= 0.8 \times (5/48) \times 9142.86 \times (10 \times 12)^2 / (3408788 \times 1632.1) \\
 &= \mathbf{0.001972''} \\
 \Delta_{iSUS} &= K (5/48) M_{SUS} \times L^2 / (E_c \times I_e) \\
 &= 0.8 \times (5/48) \times 16868.0 \times (10 \times 12)^2 / (3408788 \times 1632.1) \\
 &= \mathbf{0.003638''}
 \end{aligned}$$

Allowable Deflections

$$\begin{aligned}
 \Delta_{i \text{ Allow LL}} &= (L \times 12) / \Delta_{\text{Factor Total}} \\
 &= (10 \times 12) / 180 \\
 &= \mathbf{0.6666''} \\
 &> \Delta_{iLL} = \mathbf{0.001972''} \quad \text{(OK)}
 \end{aligned}$$

8.3.2.3.2 Long term Deflection

i. Sustained load duration of 5 years & more

$$\begin{aligned}
 \lambda &= \xi / (1 + 50 \times p') \\
 &= 2.0 / (1 + 50 \times 0.0035) \\
 &= \mathbf{1.702} \\
 \Delta_{(CP+SH)} &= \lambda \times \Delta_{iSUS} \\
 &= \mathbf{1.702 \times 0.003638} \\
 &= \mathbf{0.006192 \text{ in}} \\
 \Delta_{(CP+SH)} + \Delta_{iLL} &= \mathbf{0.006192 + 0.001972} \\
 &= \mathbf{0.008164 \text{ in}}
 \end{aligned}$$

Allowable Deflections

$$\begin{aligned}
 \Delta_{i \text{ Allow}} &= (L \times 12) / \Delta_{\text{Factor}} \\
 &= (10 \times 12) / 240 \\
 &= \mathbf{0.5''} \\
 &> \mathbf{0.008164''} \quad \text{(OK)}
 \end{aligned}$$

ii. Sustained load duration of 3 Months

$$\begin{aligned}\text{Sustained Moment, } M_{\text{SUS}} &= M_D + 0.5 \times M_L \quad (\text{Assume that 50\% Load as sustained}) \\ &= 12296.57 + 0.5 \times 9142.86 \\ &= 16868 \text{ lb-in}\end{aligned}$$

Under Sustained Load

$$\begin{aligned}M_{\text{cr}} / M_{\text{SUS}} &= 88800.9 / 16868 \\ &= 5.264\end{aligned}$$

$$\text{Hence } (I_e)_d = I_g$$

$$\begin{aligned}\lambda &= \xi / (1 + 50 \times p') \\ &= 1.0 / (1 + 50 \times 0.0035) \\ &= 0.851\end{aligned}$$

$$\begin{aligned}\Delta_{(\text{CP+SH})} &= \lambda \times \Delta_{i \text{ SUS}} \\ &= 0.851 \times 0.003638 \\ &= 0.003096 \text{ in}\end{aligned}$$

$$\begin{aligned}\Delta_{(\text{CP+SH})} + \Delta_{i \text{ LL}} &= 0.003096 + 0.001972 \\ &= 0.005068 \text{ in}\end{aligned}$$

Allowable Deflections

$$\begin{aligned}\Delta_{i \text{ Allow}} &= (L \times 12) / \Delta_{\text{Factor}} \\ &= (10 \times 12) / 240 \\ &= 0.5'' \\ &> 0.005068'' \quad (\text{OK})\end{aligned}$$

8.3.3 Calculation for Transverse Slab Reinforcement

Consider 12" width of slab,

$$L_{\text{Slab}} = 27.5 / 12 = 2.292 \text{ ft}$$

$$\text{Self weight of deck} = 116.794 \text{ (As calculated above)}$$

$$\begin{aligned} \text{Total factored load, } P_U &= 1.2 \times 10 \times 12 / 12 + 1.2 \times 116.794 + 1.6 \times 40 \times 12 / 12 \\ &= 216.15 \text{ plf} \end{aligned}$$

$$\begin{aligned} \text{Maximum Moment} &= 216.15 \times 2.29^2 / 12 \\ &= 94.4 \text{ ft-lb} \\ &= 1133.5 \text{ in-lb} \end{aligned}$$

$$\begin{aligned} \text{Tension controlled reinforcement ratio } (\rho_t) &= 0.319 \times 0.85 \times 3500 / 60000 \\ &= 0.0158 \end{aligned}$$

$$\begin{aligned} \text{Maximum allowed reinforcement ratio } (\rho_{\text{Max}}) &= \rho_t \\ &= 0.0158 \end{aligned}$$

$$\begin{aligned} \text{Minimum reinforcement ratio } (\rho_{\text{Min}}) &= \text{Max } (3 \times (f'c)^{0.5}, 200) / f_y \\ &= \text{Max } (3 \times (3500)^{0.5}, 200) / 60000 \\ &= \text{Max } (177.5, 200) / 60000 \\ &= 200 / 60000 \\ &= 0.0033 \end{aligned}$$

Reinforcement ratio for +ive moment (ρ_{Pos})

$$\begin{aligned} &= (0.85 \times f'c / f_y) \times \{1 - [1 - 2 \times M_{UP} / (\phi \times b_w \times t_f / 2^2 \times 0.85 \times f'c)]^{0.5}\} \\ &= 1.78 \times 10^{-3} \\ &= 0.00178 < (\rho_{\text{Min}} = 0.0033) \\ &= 0.00178 < (\rho_{\text{Max}} = 0.0158) \text{ OK} \end{aligned}$$

$$\begin{aligned} \text{Area of Reinforcement Required} &= 0.00178 \times 12 \times 2/2 \\ &= 0.021 \text{ in}^2 \end{aligned}$$

Rebar Used = #4 rebar

$$\text{Area of Rebar} = 0.1963 \text{ in}^2$$

$$\begin{aligned} \text{Spacing} &= (0.1963 / 0.021) \times 12 \\ &= 112.71 \text{ in} \end{aligned}$$

Per Section 7.12 of ACI-318-02 Spacing of rebar will be Minimum of the following three

- (1) Calculated spacing as above = 112.71 in
- (2) 5 times of thickness of slab = 5 x 2 = 10 in
- (3) 18 in

Provide #4 rebar @ 10" O.C.

8.3.4 Calculation for Longitudinal Slab Reinforcement

Consider 12" width of slab,

$$\begin{aligned} \text{Per Section 7.12 of ACI-318-02 Minimum reinforcement} &= 0.0018 \times \text{area of cross section} \\ &= 0.0018 \times 2 \times 12 \end{aligned}$$

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Date: 05/01/2007

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$$\begin{aligned} &= 0.0432 \text{ in} \\ \text{Spacing} &= (0.1963 / 0.0432) \times 12 \\ &= 54.52 \text{ in} \end{aligned}$$

Per Section 7.12 of ACI-318-02 Spacing of rebar will be Minimum of the following three

- (1) Calculated spacing as above = 54.52 in
- (2) 5 times of thickness of slab = $5 \times 2 = 10$ in
- (3) 18 in

Provide #4 rebar @ 10" O.C.

9 AmDeck Joist Design Chart

9.1 Table A: f'c = 3500 psi, Topping Thickness = 2.0"

General Data:

Unit weight of concrete = 145 pcf

Δ_i LL = 180

Panel Size = 12"

Δ_i TOTAL = 240

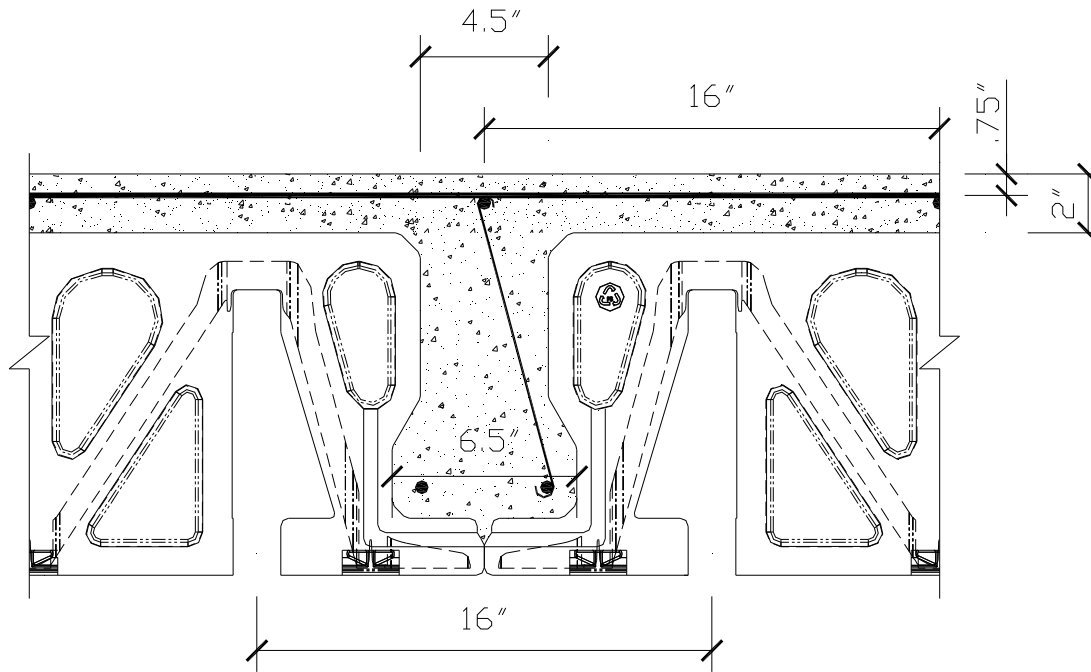
Floor Size: 12" + 2"

Rebar strength = 60000 psi

Dead Load Factor = 1.2

2" Standard insulation

Live Load Factor = 1.6



9.2 Table B: $f'c = 3500$ psi, Topping Thickness = 2.5"

General Data:

Unit weight of concrete = 145 pcf

Δ_i LL = 180

Panel Size = 12"

Δ_i TOTAL = 240

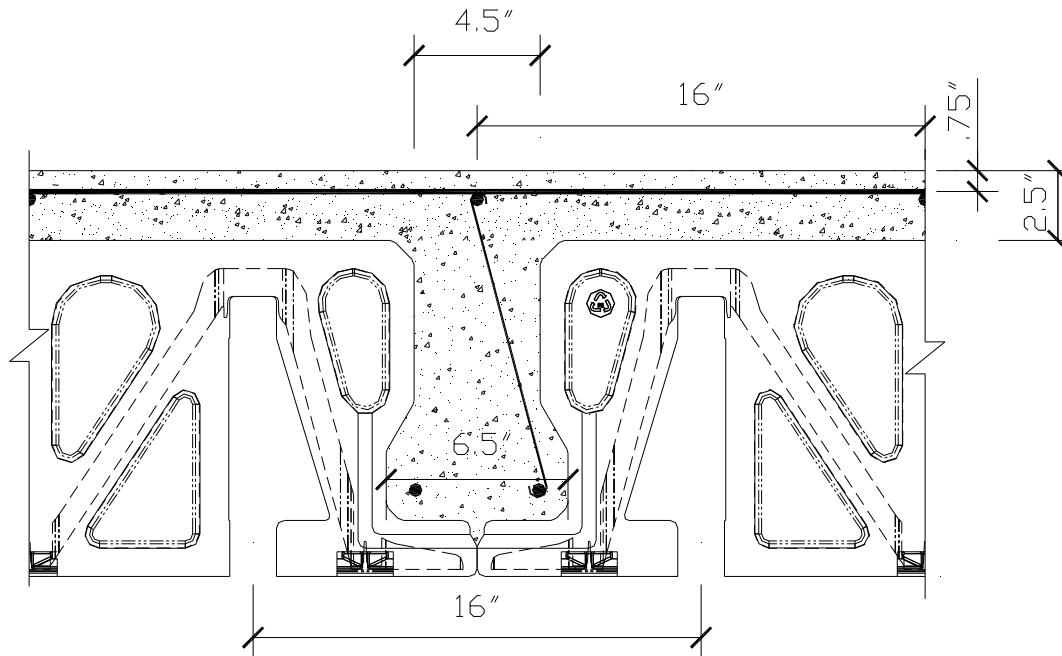
Floor Size: 12" + 2.5"

Rebar strength = 60000 psi

Dead Load Factor = 1.2

2" Standard insulation

Live Load Factor = 1.6



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Dead Load = 10 psf

Span	M	D	1 - 9' 0" - 11'			1 - 9' 0" - 11'			1 - 9' 0" - 11'			1 - 9' 0" - 11'			1 - 9' 0" - 11'			1 - 9' 0" - 11'				
			SP	DF	VS	SP	DF	VS	SP	DF	VS	SP	DF	VS	SP	DF	VS	SP	DF	VS		
11	Full	End Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	
		HL Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Landed	Full Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Other HL Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
Revised Section																						
17	Full	End Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		HL Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Landed	Full Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Other HL Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
Revised Section																						
14	Full	End Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		HL Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Landed	Full Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Other HL Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
Revised Section																						
16	Full	End Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		HL Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Landed	Full Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Other HL Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
Revised Section																						
18	Full	End Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		HL Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Landed	Full Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Other HL Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
Revised Section																						
20	Full	End Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		HL Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Landed	Full Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Other HL Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
Revised Section																						
24	Full	End Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		HL Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Landed	Full Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Other HL Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
Revised Section																						
30	Full	End Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		HL Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Landed	Full Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Other HL Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
Revised Section																						
36	Full	End Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		HL Slab	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Landed	Full Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Other HL Support	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
Revised Section																						

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Date: 12/07/2007

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Dead Load = 15 psf

Bay	Type	Support	1 - 2			2 - 3			3 - 4			4 - 5			5 - 6			6 - 7		
			DL	LL	UL	DL	LL	UL	DL	LL	UL	DL	LL	UL	DL	LL	UL	DL	LL	UL
1L	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
1T	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
1B	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
1F	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
1R	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
2	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
24	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
3	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
36	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150
	Full Deck	Full Deck	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150	140	150	150

Notes

- Shaded portion value shows that joists are provide with shear reinforcement w/ #3 rebar single leg @ 5" O.C.
- Blank Cells indicates that the joists are failing in deflection.

9.3 Table C: $f'c = 3500$ psi, Topping Thickness = 3.0"

General Data:

Unit weight of concrete = 145 pcf

Δ_i LL = 180

Panel Size = 12"

Δ_i TOTAL = 240

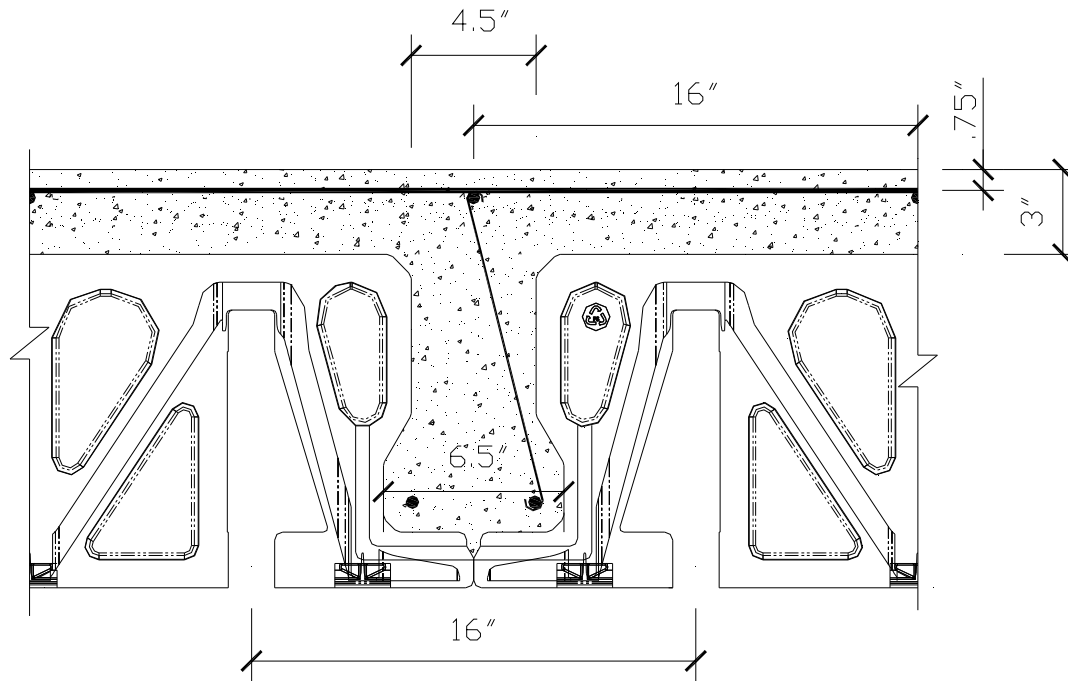
Floor Size: 12" + 3"

Rebar strength = 60000 psi

Dead Load Factor = 1.2

2" Standard insulation

Live Load Factor = 1.6



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Checked by: Andy / Raj

Date: 12/07/2007

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Dead Load = 15 psf

Span	M	SF	1 - 5' 0" - 1'			1 - 5' 0" - 1'			1 - 5' 0" - 1'			1 - 5' 0" - 1'			1 - 5' 0" - 1'			1 - 5' 0" - 1'		
			DF	DF	DF	DF	DF	DF	DF	DF	DF	DF	DF	DF	DF	DF	DF	DF	DF	DF
11	Sum	Full Slabs	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Slabs	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Load	Full Slabs	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Slabs	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
17	Sum	Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
		Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
	Load	Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
		Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
14	Sum	Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
		Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
	Load	Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
		Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
16	Sum	Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
		Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
	Load	Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
		Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
18	Sum	Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
		Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
	Load	Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
		Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
20	Sum	Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
		Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
	Load	Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
		Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
24	Sum	Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
		Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
	Load	Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
		Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
26	Sum	Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
		Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
	Load	Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145
		Full Slabs	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145	145

Notes

- Shaded portion value shows that joists are provide with shear reinforcement w/ #3 rebar single leg @ 5" O.C.
- Blank Cells indicates that the joists are failing in deflection.

9.4 Table D: f'c = 3500 psi, Topping Thickness = 3.5"

General Data:

Unit weight of concrete = 145 pcf

Δ_i_{LL} = 180

Panel Size = 12"

Δ_i_{TOTAL} = 240

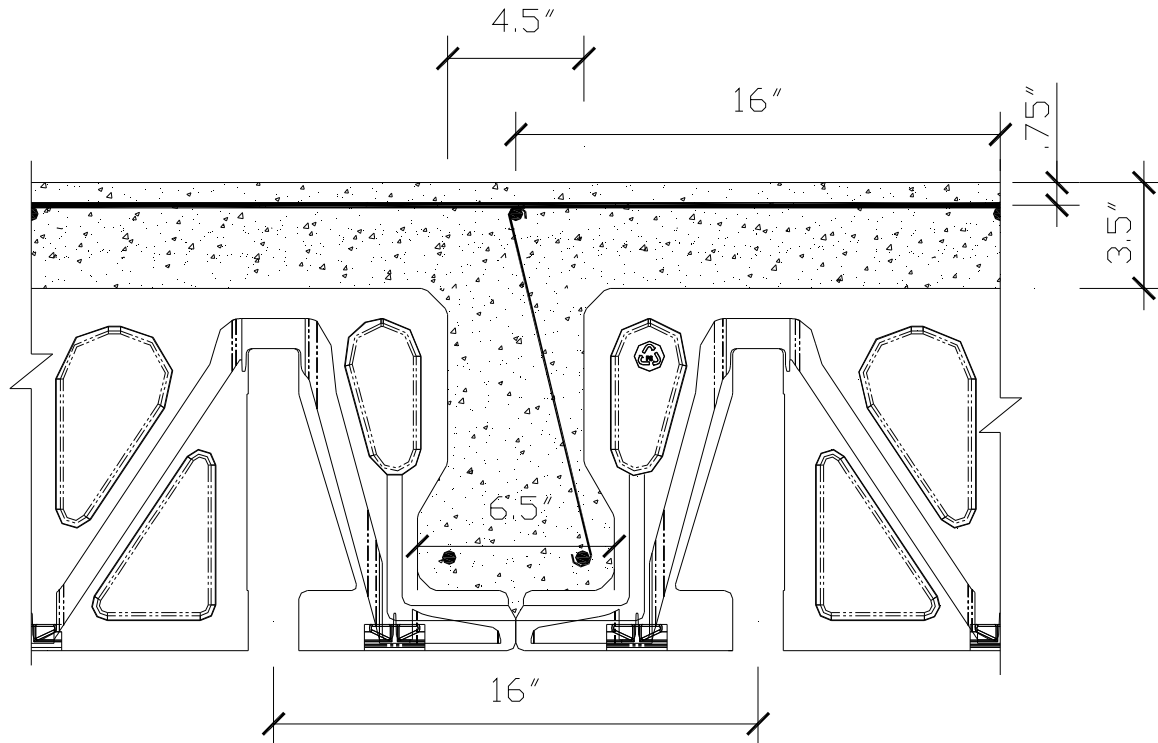
Floor Size: 12" + 3.5"

Rebar strength = 60000 psi

Dead Load Factor = 1.2

2" Standard insulation

Live Load Factor = 1.6



Consulting Engineers, Corp

Project: AmDeck Design Guide

Client: Amvic, Inc.

Prepared by: Kapil

Checked by: Andy / Raj

Date: 12/07/2007

Date: 12/07/2007

Dead Load = 15 psf

Bay	Span	Type	1 - 2			2 - 3			3 - 4			4 - 5			5 - 6			6 - 7			
			SP	DP	US	SP	DP	US	SP	DP	US	SP	DP	US	SP	DP	US	SP	DP	US	
1	1	Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
1	2	Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
1	3	Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
1	4	Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
1	5	Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
1	6	Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
1	7	Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
		Full Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140

Notes

- Shaded portion value shows that joists are provide with shear reinforcement w/ #3 rebar single leg @ 5" O.C.
- Blank Cells indicates that the joists are failing in deflection.

9.5 Table E: f'c = 3500 psi, Topping Thickness = 4.0"

General Data:

Unit weight of concrete = 145 pcf

Δ_i LL = 180

Panel Size = 12"

Δ_i TOTAL = 240

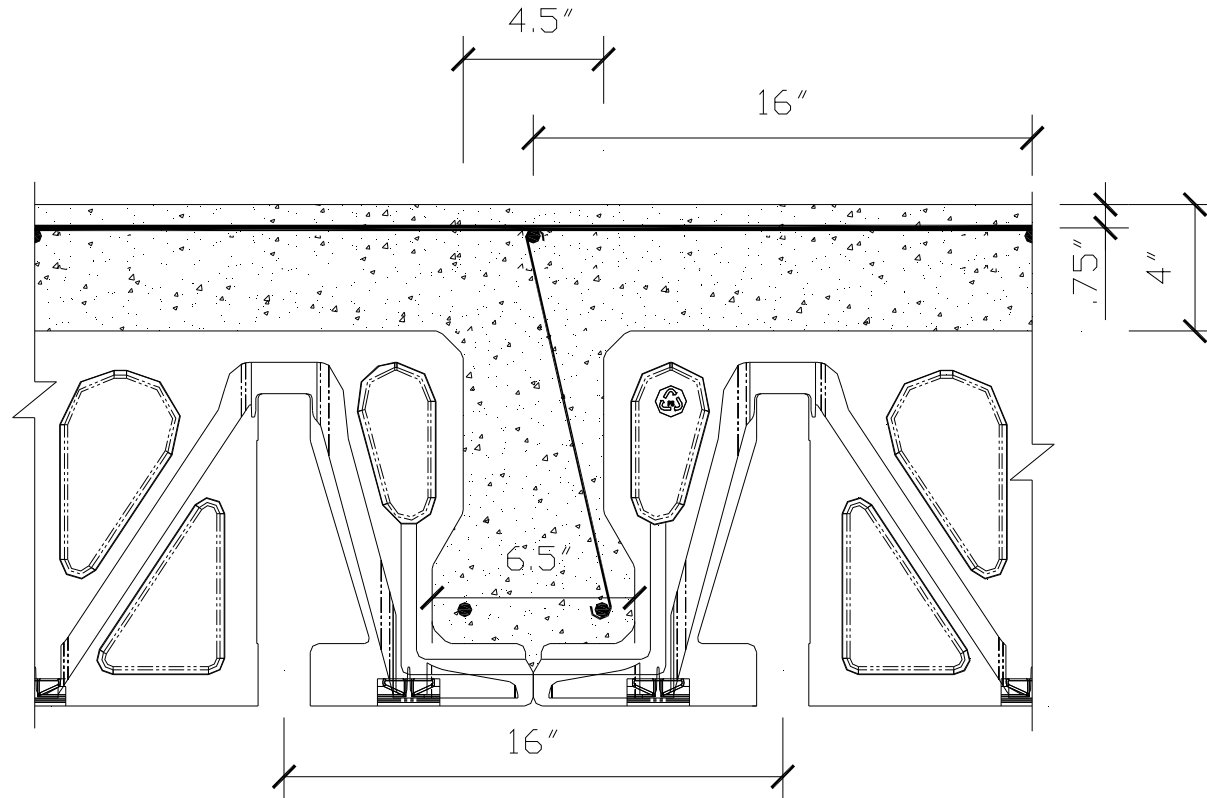
Floor Size: 12" + 4"

Rebar strength = 60000 psi

Dead Load Factor = 1.2

2" Standard insulation

Live Load Factor = 1.6



Consulting Engineers, Corp

Project: AmDeck Design Guide

Client: Amvic, Inc.

Prepared by: Kapil

Checked by: Andy / Raj

Date: 12/07/2007

Date: 12/07/2007

Dead Load = 15 psf

Span	ft	3500	LL=50 DL=15			LL=50 DL=15			LL=60 DL=15			LL=70 DL=15			LL=80 DL=15			LL=90 DL=15			LL=100 DL=15			
			SS	DS	MS	SS	DS	MS	SS	DL	MS	SS	DS	MS	SS	DS	MS	SS	DS	MS	SS	DS	MS	
10	Bottom Reinforcement	End Spans	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
		Int. Spans	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
		1 st Int. Support	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
12	Bottom Reinforcement	End Spans	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	
		Int. Spans	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
		1 st Int. Support	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
14	Bottom Reinforcement	End Spans	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	
		Int. Spans	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
		1 st Int. Support	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
16	Bottom Reinforcement	End Spans	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	
		Int. Spans	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	1#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
		1 st Int. Support	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4
18	Bottom Reinforcement	End Spans	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	
		Int. Spans	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
		1 st Int. Support	1#4	2#4	1#5	1#4	2#4	1#5	1#4	2#4	1#5	1#4	2#4	1#5	1#4	2#4	1#5	1#4	2#4	1#5	1#4	2#4	1#5	1#4
20	Bottom Reinforcement	End Spans	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
		Int. Spans	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
		1 st Int. Support	1#4	1#4+1#5	1#5	1#4	1#4+1#5	1#5	1#4	1#4+1#5	1#5	1#4	1#4+1#5	1#5	1#4	1#4+1#5	1#5	1#4	1#4+1#5	1#5	1#4	1#4+1#5	1#5	1#4
22	Bottom Reinforcement	End Spans	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	
		Int. Spans	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
		1 st Int. Support	1#4	1#4+1#5	1#5	1#4	1#4+1#5	1#5	1#4	1#4+1#5	1#5	1#4	1#4+1#5	1#5	1#4	1#4+1#5	1#5	1#4	1#4+1#5	1#5	1#4	1#4+1#5	1#5	1#4
24	Bottom Reinforcement	End Spans	1#5+1#6	2#4	2#4	1#5+1#6	2#4	2#4	1#5+1#6	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	
		Int. Spans	1#5+1#6	2#4	2#4	1#5+1#6	2#4	2#4	1#5+1#6	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4	2#4	1#4	2#4	2#4	1#4	2#4	2#4	1#4	2#4	2#4	1#4	2#4	2#4	1#4	2#4	2#4	1#4	2#4	2#4	1#4
		1 st Int. Support	1#4	2#5	2#5	1#4	2#5	2#5	1#4	1#5+1#6	2#5	1#4	1#5+1#6	2#5	1#4	1#5+1#6	2#5	1#4	1#5+1#6	2#5	1#4	1#5+1#6	2#5	1#4
26	Bottom Reinforcement	End Spans	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	
		Int. Spans	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4	2#4	1#4	2#4	2#4	1#4	2#4	2#4	1#4	2#4	2#4	1#4	2#4	2#4	1#4	2#4	2#4	1#4	2#4	2#4	1#4
		1 st Int. Support	1#4	1#5+1#6	1#5+1#6	1#4	1#5+1#6	1#5+1#6	1#4	1#5+1#6	1#5+1#6	1#4	1#5+1#6	1#5+1#6	1#4	1#5+1#6	1#5+1#6	1#4	1#5+1#6	1#5+1#6	1#4	1#5+1#6	1#5+1#6	1#4
28	Bottom Reinforcement	End Spans	1#5+1#7	2#5	2#5	1#5+1#7	2#5	2#5	1#5+1#7	2#5	2#5	1#5+1#7	2#5	2#5	1#5+1#7	2#5	2#5	1#5+1#7	2#5	2#5	1#5+1#7	2#5	2#5	
		Int. Spans	1#5+1#7	2#5	2#5	1#5+1#7	2#5	2#5	1#5+1#7	2#5	2#5	1#5+1#7	2#5	2#5	1#5+1#7	2#5	2#5	1#5+1#7	2#5	2#5	1#5+1#7	2#5	2#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4+1#5	1#4+1#5	1#4	1#4+1#5	1#4+1#5	1#4	1#4+1#5	1#4+1#5	1#4	1#4+1#5	1#4+1#5	1#4	1#4+1#5	1#4+1#5	1#4	1#4+1#5	1#4+1#5	1#4	1#4+1#5	1#4+1#5	1#4
		1 st Int. Support	1#4	2#5	2#5	1#4	2#5	2#5	1#4	1#5+1#6	2#5	1#4	1#5+1#6	2#5	1#4	1#5+1#6	2#5	1#4	1#5+1#6	2#5	1#4	1#5+1#6	2#5	1#4
30	Bottom Reinforcement	End Spans	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	
		Int. Spans	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	2#5	2#5	1#4	2#5	2#5	1#4	2#5	2#5	1#4	2#5	2#5	1#4	2#5	2#5	1#4	2#5	2#5	1#4	2#5	2#5	1#4
		1 st Int. Support	1#4	1#5+1#6	1#5+1#6	1#4	1#5+1#6	1#5+1#6	1#4	1#5+1#6	1#5+1#6	1#4	1#5+1#6	1#5+1#6	1#4	1#5+1#6	1#5+1#6	1#4	1#5+1#6	1#5+1#6	1#4	1#5+1#6	1#5+1#6	1#4

Notes

- Shaded portion value shows that joists are provide with shear reinforcement w/ #3 rebar single leg @ 5" O.C.
- Blank Cells indicates that the joists are failing in deflection.

9.6 Table F: $f'c = 3500$ psi, Topping Thickness = 4.5"

General Data:

Unit weight of concrete = 145 pcf

Panel Size = 12"

Floor Size: 12" + 4.5"

Rebar strength = 60000 psi

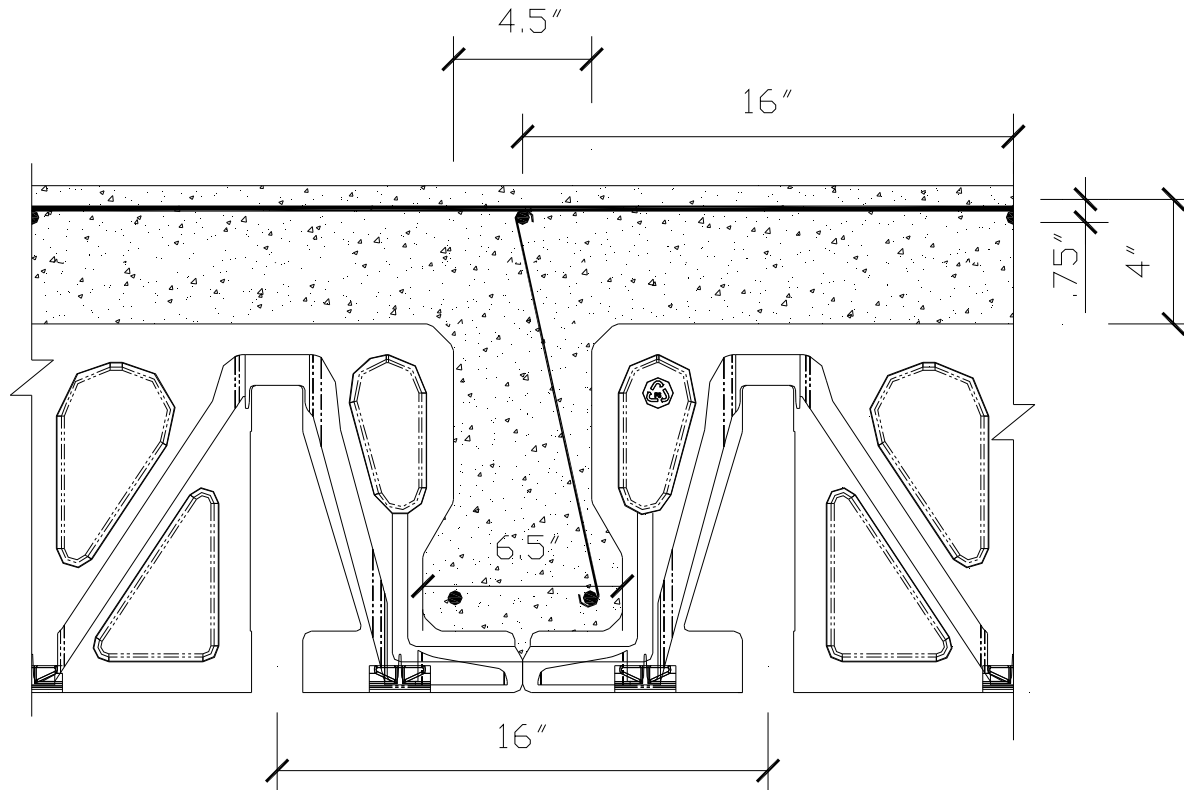
2" Standard insulation

$\Delta_i_{LL} = 180$

$\Delta_i_{TOTAL} = 240$

Dead Load Factor = 1.2

Live Load Factor = 1.6



9.7 Table G: $f'c = 4000$ psi, Topping Thickness = 2.0"

General Data:

Unit weight of concrete = 145 pcf

Δ_i LL = 180

Panel Size = 12"

Δ_i TOTAL = 240

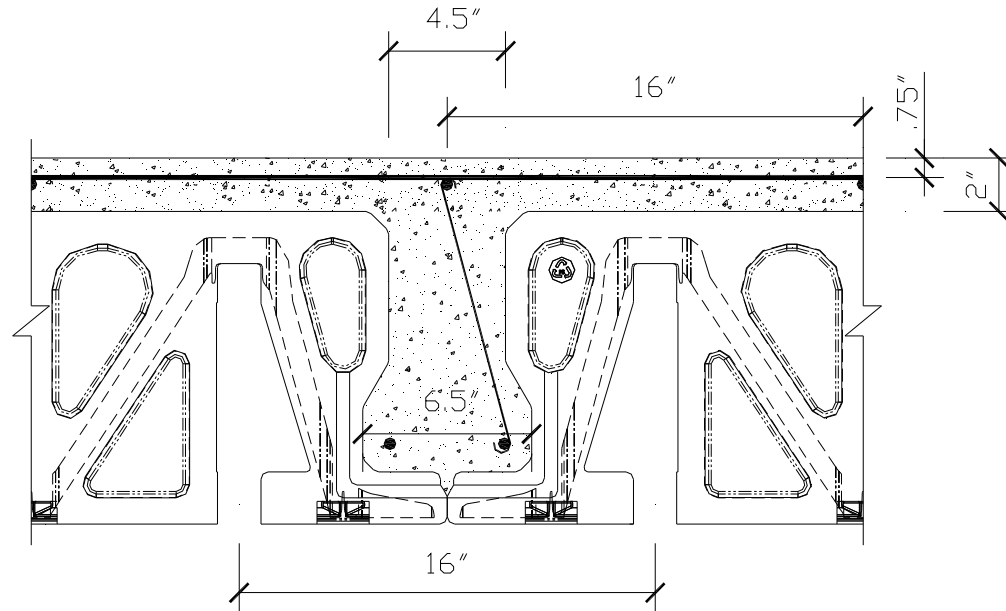
Floor Size: 12" + 2"

Rebar strength = 60000 psi

Dead Load Factor = 1.2

2" Standard insulation

Live Load Factor = 1.6



Consulting Engineers, Corp

Project: AmDeck Design Guide

Client: Amvic, Inc.

Prepared by: Kapil

Checked by: Andy / Raj

Date: 12/07/2007

Date: 12/07/2007

Dead Load = 15 psf

Span	Type	1 - 5' 0" - 1'			1 - 5' 0" - 1'			1 - 5' 0" - 1'			1 - 5' 0" - 1'			1 - 5' 0" - 1'			1 - 5' 0" - 1'			1 - 5' 0" - 1'			
		SP	DF	VS	SP	DF	VS	SP	DF	VS	SP	DF	VS	SP	DF	VS	SP	DF	VS	SP	DF	VS	
11	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
17	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
14	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
16	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
18	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
20	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
24	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
30	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
	Full Service	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140

Notes

- Shaded portion value shows that joists are provide with shear reinforcement w/ #3 rebar single leg @ 5" O.C.
- Blank Cells indicates that the joists are failing in deflection.

9.8 Table H: f'c = 4000 psi, Topping Thickness = 2.5"

General Data:

Unit weight of concrete = 145 pcf

Δ_i LL = 180

Panel Size = 12"

Δ_i TOTAL = 240

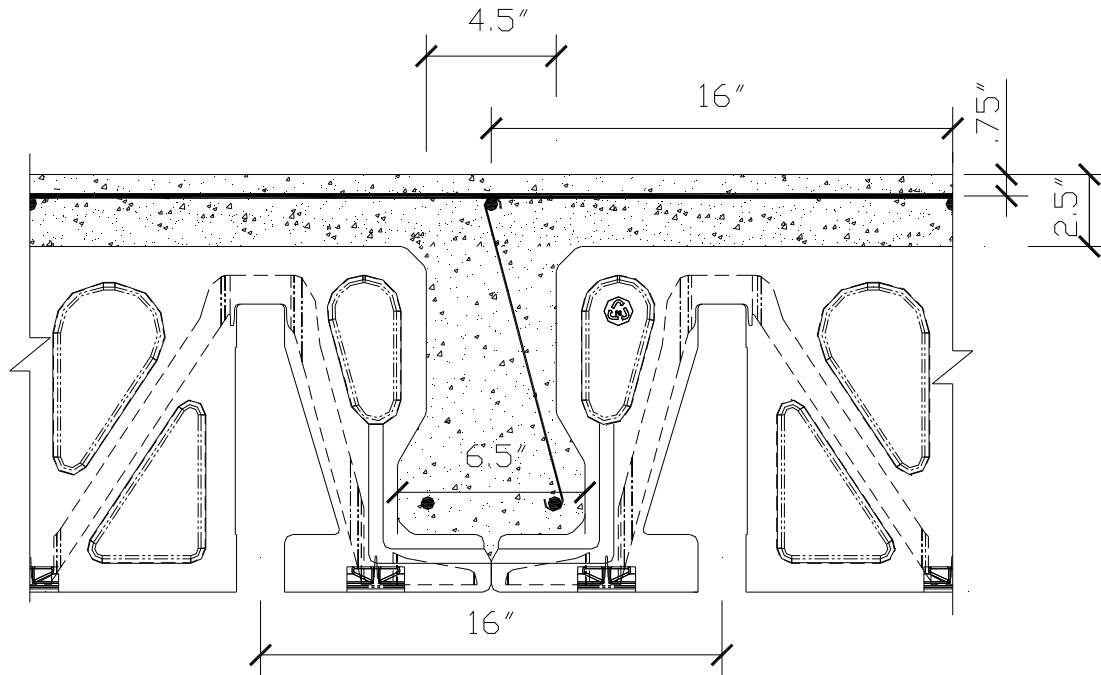
Floor Size: 12" + 2.5"

Rebar strength = 60000 psi

Dead Load Factor = 1.2

2" Standard insulation

Live Load Factor = 1.6



Consulting Engineers, Corp

Project: AmDeck Design Guide

Client: Amvic, Inc.

Prepared by: Kapil

Checked by: Andy / Raj

Date: 12/07/2007

Date: 12/07/2007

Dead Load = 10 psf

Span	fc	4000	LL=50 DL=10			LL=60 DL=10			LL=60 DL=10			LL=70 DL=10			LL=80 DL=10			LL=90 DL=10			LL=100 DL=10			
			SS	DS	MS	SS	DS	MS	SS	DS	MS	SS	DS	MS	SS	DS	MS	SS	DS	MS	SS	DS	MS	
10	Bottom Reinforcement	End Spans	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
		Int. Spans	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
		1 st Int. Support	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
	Other Int. Support Slab	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
12	Bottom Reinforcement	End Spans	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	
		Int. Spans	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
		1 st Int. Support	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
	Other Int. Support Slab	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
14	Bottom Reinforcement	End Spans	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	
		Int. Spans	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
		1 st Int. Support	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
	Other Int. Support Slab	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
16	Bottom Reinforcement	End Spans	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	
		Int. Spans	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
		1 st Int. Support	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
	Other Int. Support Slab	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
18	Bottom Reinforcement	End Spans	2#4	1#4	1#4	2#4	1#4	1#4	2#4	1#5	1#5	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	
		Int. Spans	2#4	1#4	1#4	2#4	1#4	1#4	2#4	1#5	1#5	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
		1 st Int. Support	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
	Other Int. Support Slab	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	
20	Bottom Reinforcement	End Spans	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	2#5	1#5	1#5	2#5	2#4	2#4	1#5+1#5	2#4	2#4	1#5+1#5	2#4	2#4	
		Int. Spans	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	1#4+1#5	1#5	1#5	2#5	1#5	1#5	2#5	2#4	2#4	1#5+1#5	2#4	2#4	1#5+1#5	2#4	2#4	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
		1 st Int. Support	1#4	2#4	2#4	1#4	2#4	2#4	1#4	1#4+1#5	2#4	1#4	1#4+1#5	2#4	1#4	1#4+1#5	1#4	2#5	1#4+1#5	1#4	2#5	1#4+1#5	1#4	2#5
	Other Int. Support Slab	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4+1#5	1#4	1#4	1#5	1#4	1#5	
22	Bottom Reinforcement	End Spans	2#5	1#5	1#5	2#5	1#5	1#5	2#5	2#4	2#4	1#5+1#5	2#4	2#4	1#5+1#5	2#4	2#4	2#5	1#4+1#5	2#5	1#4+1#5	2#5	1#4+1#5	
		Int. Spans	2#5	1#5	1#5	2#5	1#5	1#5	2#5	2#4	2#4	1#5+1#5	2#4	2#4	1#5+1#5	2#4	2#4	2#5	1#4+1#5	2#5	1#4+1#5	2#5	1#4+1#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
		1 st Int. Support	1#4	1#4+1#5	1#4+1#5	1#4	1#4+1#5	1#4+1#5	1#4	2#5	1#4+1#5	1#4	2#5	1#4+1#5	1#4	2#5	2#5	1#4	1#5+1#5	2#5	1#4	1#5+1#5	2#5	1#4+1#5
	Other Int. Support Slab	1#4	1#4	2#4	1#4	1#4	2#4	1#4	1#4	2#4	1#4	1#4+1#5	1#4	1#4	1#4+1#5	1#4	1#4	1#4+1#5	1#4	1#4	2#5	1#4	2#5	
24	Bottom Reinforcement	End Spans	1#5+1#5	2#4	2#4	1#5+1#5	2#4	2#4	1#5+1#5	2#4	2#4	2#5	1#4+1#5	1#4+1#5	2#5	2#5	1#4+1#5	1#5+1#5	2#4	2#4	1#5+1#5	2#4	2#4	
		Int. Spans	1#5+1#5	2#4	1#5	1#5+1#5	2#4	1#5	1#5+1#5	2#4	2#4	2#5	1#4+1#5	1#4+1#5	2#5	2#5	1#4+1#5	1#5+1#5	2#4	2#4	1#5+1#5	2#4	2#4	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
		1 st Int. Support	1#4	2#5	1#5	1#4	2#5	1#4+1#5	1#4	1#5+1#5	2#5	1#4	1#5+1#5	1#4	1#5+1#5	1#4	2#5	1#4	1#5+1#5	1#4	1#5+1#5	1#4	1#5+1#5	
	Other Int. Support Slab	1#4	1#4	1#4+1#5	1#4	1#4	1#4+1#5	1#4	1#4	1#4+1#5	1#4	1#4	1#4+1#5	1#4	1#4	1#4+1#5	1#4	1#4	1#4+1#5	1#4	1#4	1#5+1#5	1#4	1#5+1#5
26	Bottom Reinforcement	End Spans	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	2#5	1#4+1#5	1#4+1#5	1#5+1#7	2#5	2#5	2#7	2#5	2#5	2#5	1#4+1#5	2#7	2#5	1#5+1#5	1#5+1#5	
		Int. Spans	2#5	1#4+1#5	1#4	2#5	1#4+1#5	1#4	2#5	1#4+1#5	1#4+1#5	1#5+1#7	2#5	2#5	2#7	2#5	2#5	2#5	1#4+1#5	2#7	2#5	1#5+1#5	1#5+1#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4	2#4	1#4	2#4	1#4	1#4	2#4	1#4	1#4+1#5	1#4	1#4	1#4+1#5	1#4	1#4+1#5	1#4	1#4+1#5	1#4	1#4	1#5+1#7	1#4	2#7
		1 st Int. Support	1#4	1#5+1#5	2#5	1#4	1#5+1#5	2#5	1#4	1#5+1#5	2#5	1#4	1#5+1#5	1#4	1#5+1#5	1#4	1#5+1#7	2#5	1#4	1#5+1#7	1#4	2#7	1#5+1#7	1#4
	Other Int. Support Slab	1#4	1#4	2#5	1#4	1#4	2#5	1#4	1#4	2#5	1#4	1#4	2#5	1#4	1#4	1#5+1#5	1#4	1#5+1#7	2#5	1#4	1#5+1#7	1#4	2#5	
28	Bottom Reinforcement	End Spans	1#5+1#7	1#4+1#5	1#4+1#5	1#5+1#7	1#4+1#5	1#4+1#5	1#5+1#7	2#5	2#5	1#5+1#7	2#5	2#5	2#7	1#5+1#5	2#5	2#7	1#5+1#5	2#7	1#5+1#5	2#5	2#5	
		Int. Spans	1#5+1#7	1#4+1#5	1#4+1#5	1#5+1#7	1#4+1#5	1#4+1#5	1#5+1#7	2#5	2#5	1#5+1#7	2#5	2#5	2#7	1#5+1#5	2#5	2#7	1#5+1#5	2#7	1#5+1#5	2#5	2#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4+1#5	1#4+1#5	1#4	1#4+1#5	1#4+1#5	1#4	1#4+1#5	1#4	1#4+1#5	1#4	1#4+1#5	1#4	1#4+1#5	1#4	1#5+1#7	1#4	1#5+1#7	1#4	1#4	1#5+1#7	
		1 st Int. Support	1#4	2#5	1#5+1#5	1#4	2#5	1#5+1#5	1#4	1#5+1#7	2#5	1#4	1#5+1#7	2#5	1#4	1#5+1#7	2#5	1#4	1#5+1#7	1#4	1#4	1#5+1#7	1#4	1#5+1#7
	Other Int. Support Slab	1#4	1#4	1#5+1#5	1#4	1#4	1#5+1#5	1#4	1#4	1#5+1#5	1#4	1#4	1#5+1#5	1#4	1#4	1#5+1#5	1#4	1#4	1#5+1#5	1#4	1#4	1#5+1#7	1#4	1#5+1#7
30	Bottom Reinforcement	End Spans	2#7	2#5	2#5	2#7	2#5	2#5	2#7	1#5+1#5	1#5+1#5	2#7	1#5+1#5	1#5+1#5	2#7	2#5	2#5	2#7	2#5	2#7	1#5+1#7	1#5+1#7	2#5	
		Int. Spans	2#7	2#5	1#4+1#5	2#7	2#5	1#4+1#5	2#7	1#5+1#5	2#5	2#7	1#5+1#5	1#5+1#5	2#7	1#5+1#5	2#5	2#7	2#5	2#7	1#5+1#5	1#5+1#5	2#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4+1#5	1#4+1#5	1#4	1#4+1#5	1#4+1#5	1#4	2#5	2#5	1#4	2#5	2#5	1#4	1#5+1#5	1#4	1#5+1#5	1#4	1#5+1#5	1#4	2#5	2#5	
		1 st Int. Support	1#4	1#5+1#7	2#5	1#4	1#5+1#7	2#5	1#4	2#7	1#5+1#7	1#4	2#7	1#5+1#7	1#4	2#7	1#5+1#7	1#4	2#7	1#5+1#7	1#4	2#7	2#7	
	Other Int. Support Slab	1#4	1#4	1#5+1#5	1#4	1#4	1#5+1#5	1#4	1#4	1#5+1#5	1#4	1#4	1#5+1#5	1#4	1#4	1#5+1#5	1#4	1#5+1#7	1#4	1#4	1#5+1#7	1#4	2#7	
Transverse Reinf	#4@12.5in OC	#4@																						

9.9 Table I: $f'c = 4000$ psi, Topping Thickness = 3.0"

General Data:

Unit weight of concrete = 145 pcf

Δ_i LL = 180

Panel Size = 12"

Δ_i TOTAL = 240

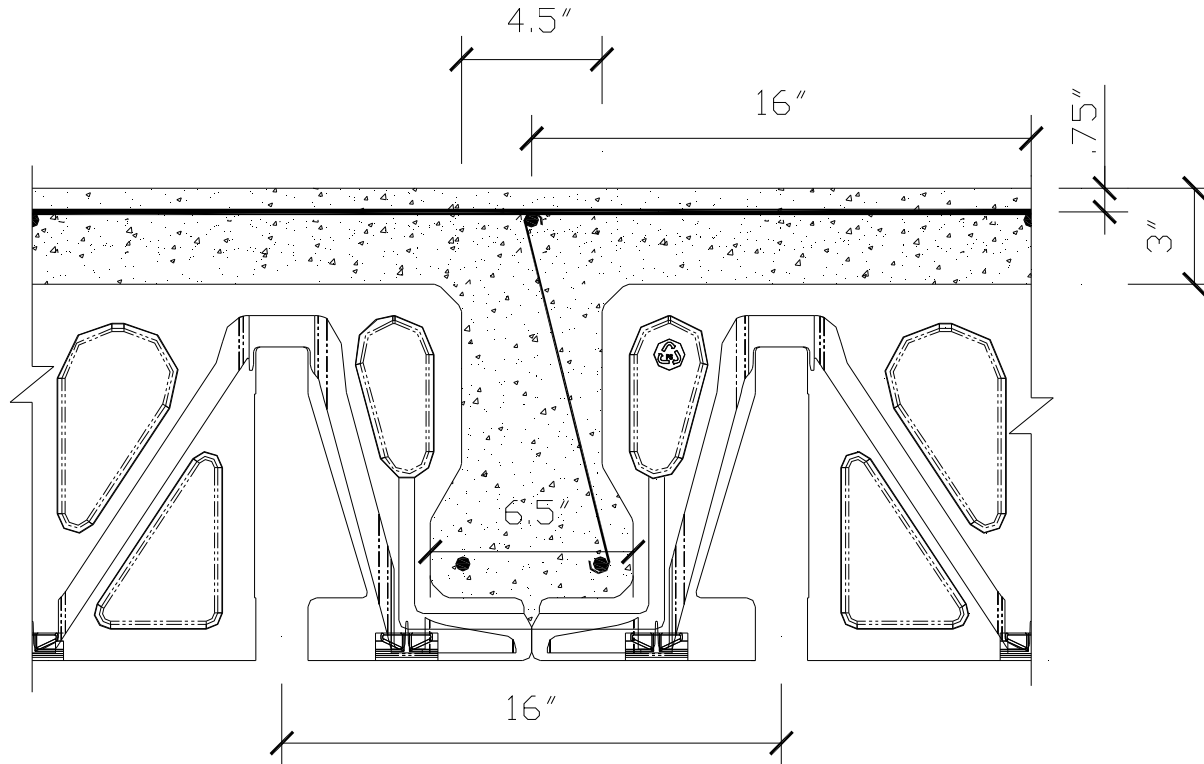
Floor Size: 12" + 3"

Rebar strength = 60000 psi

Dead Load Factor = 1.2

2" Standard insulation

Live Load Factor = 1.6



Consulting Engineers, Corp

Project: AmDeck Design Guide

Client: Amvic, Inc.

Prepared by: Kapil

Checked by: Andy / Raj

Date: 12/07/2007

Date: 12/07/2007

Dead Load = 10 psf

Span	M	D	1 - 9' 0" - 10'			1 - 9' 0" - 10'			1 - 9' 0" - 10'			1 - 9' 0" - 10'			1 - 9' 0" - 10'			1 - 9' 0" - 10'		
			SP	DF	VS	SP	DF	VS	SP	DF	VS	SP	DF	VS	SP	DF	VS	SP	DF	VS
1L	Full mem seme celed	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Uncon.dnd Deck mem	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
1'	Full mem seme celed	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Uncon.dnd Deck mem	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
14	Full mem seme celed	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Uncon.dnd Deck mem	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
16	Full mem seme celed	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Uncon.dnd Deck mem	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
1L	Full mem seme celed	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Uncon.dnd Deck mem	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
20	Full mem seme celed	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Uncon.dnd Deck mem	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
24	Full mem seme celed	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Uncon.dnd Deck mem	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
30	Full mem seme celed	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Uncon.dnd Deck mem	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
36	Full mem seme celed	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
	Uncon.dnd Deck mem	Full Deck	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
		Full Deck H. Stacks	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14

Consulting Engineers, Corp

Project: AmDeck Design Guide

Client: Amvic, Inc.

Prepared by: Kapil

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Date: 12/07/2007

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Dead Load = 15 psf

Table with 100 columns (1000 ft) and 100 rows (1000 ft). Columns are grouped by span length (4000, 1500, 1500, 600, 700, 800, 900, 1000 ft) and reinforcement type (SS, DS, MS). Rows represent different slab and support configurations (Bottom Reinforcement, Exterior Supports, 1st Int. Support, Other Int. Support, Transverse Reinf).

Notes

- Shaded portion value shows that joists are provide with shear reinforcement w/ #3 rebar single leg @ 5" O.C.
• Blank Cells indicates that the joists are failing in deflection.

9.10 Table J: $f'c = 4000$ psi, Topping Thickness = 3.5"

General Data:

Unit weight of concrete = 145 pcf

$\Delta_i LL = 180$

Panel Size = 12"

$\Delta_i TOTAL = 240$

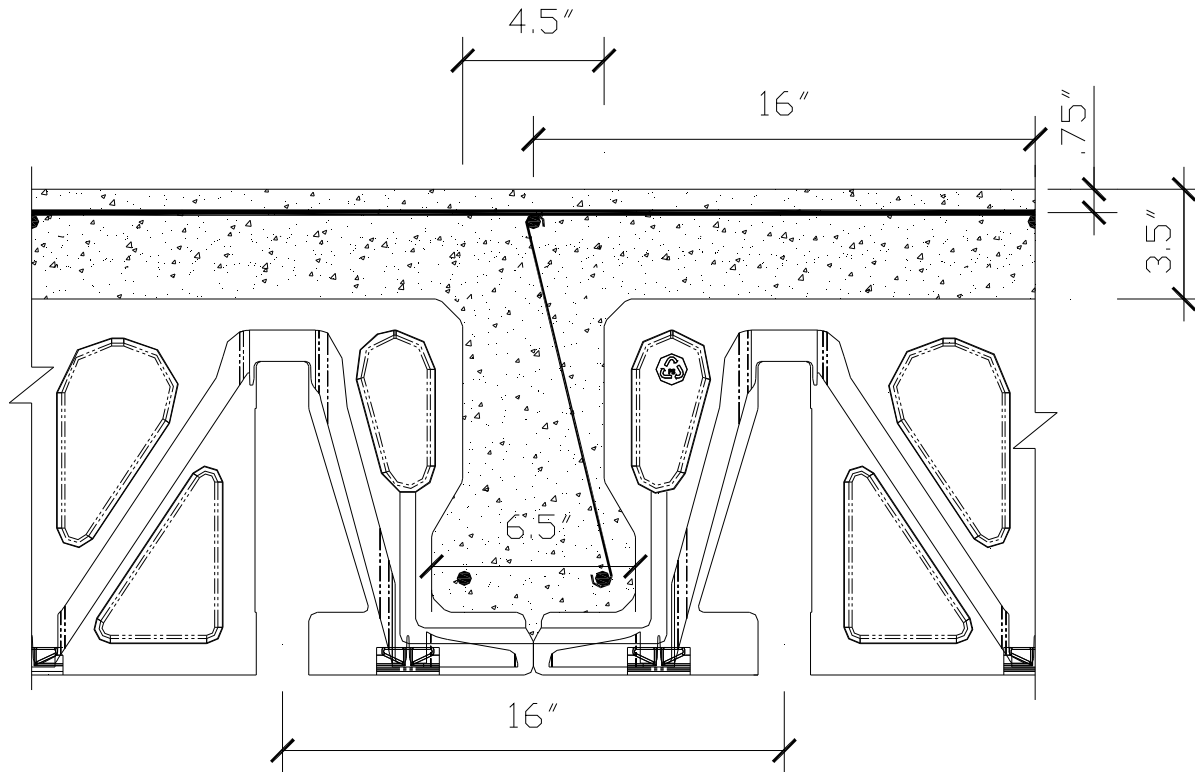
Floor Size: 12" + 3.5"

Rebar strength = 60000 psi

Dead Load Factor = 1.2

2" Standard insulation

Live Load Factor = 1.6



9.11 Table K: $f'c = 4000$ psi, Topping Thickness = 4.0"

General Data:

Unit weight of concrete = 145 pcf

Δ_i LL = 180

Panel Size = 12"

Δ_i TOTAL = 240

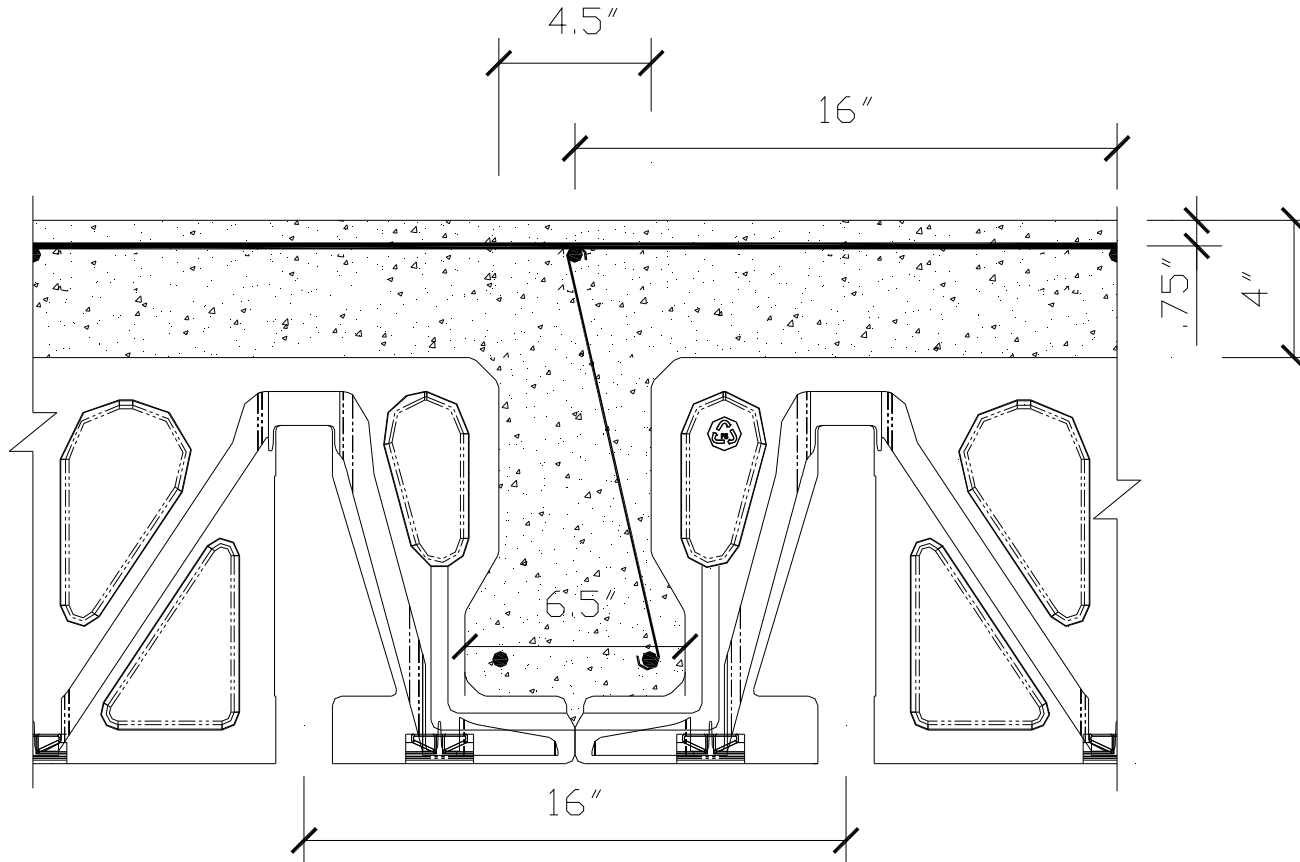
Floor Size: 12" + 4"

Rebar strength = 60000 psi

Dead Load Factor = 1.2

2" Standard insulation

Live Load Factor = 1.6



Consulting Engineers, Corp

Project: AmDeck Design Guide

Client: Amvic, Inc.

Prepared by: Kapil

Checked by: Andy / Raj

Date: 12/07/2007

Date: 12/07/2007

Dead Load = 15 psf

Span		LL=50 DL=15			LL=60 DL=15			LL=70 DL=15			LL=80 DL=15			LL=90 DL=15			LL=100 DL=15				
		SS	DS	MS	SS	DS	MS	SS	DS	MS	SS	DS	MS	SS	DS	MS	SS	DS	MS		
10	Bottom Reinforcement	End Spans	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	
		Int. Spans	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
		1 st Int. Support	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
12	Bottom Reinforcement	End Spans	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	
		Int. Spans	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
		1 st Int. Support	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
14	Bottom Reinforcement	End Spans	1#6	1#4	1#4	1#6	1#4	1#4	1#6	1#4	1#4	1#6	1#4	1#4	1#6	1#4	1#4	1#6	1#4	1#4	
		Int. Spans	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
		1 st Int. Support	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4	1#4
16	Bottom Reinforcement	End Spans	1#6	1#5	1#4	1#6	1#5	1#4	1#6	1#5	1#4	1#6	1#5	1#4	1#6	1#5	1#4	1#6	1#5	1#4	
		Int. Spans	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	
		1 st Int. Support	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	1#4	1#5	1#4	
18	Bottom Reinforcement	End Spans	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	
		Int. Spans	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	2#4	1#5	1#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
		1 st Int. Support	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
20	Bottom Reinforcement	End Spans	1#4+1#6	1#5	1#5	1#4+1#6	1#5	1#5	1#4+1#6	1#5	1#5	1#4+1#6	1#5	1#5	1#4+1#6	1#5	1#5	1#4+1#6	1#5	1#5	
		Int. Spans	1#4+1#6	1#5	1#5	1#4+1#6	1#5	1#5	1#4+1#6	1#5	1#5	1#4+1#6	1#5	1#5	1#4+1#6	1#5	1#5	1#4+1#6	1#5	1#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
		1 st Int. Support	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
22	Bottom Reinforcement	End Spans	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	
		Int. Spans	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	2#5	1#5	1#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
		1 st Int. Support	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
24	Bottom Reinforcement	End Spans	1#5+1#7	1#4+1#6	1#4+1#6	1#5+1#7	1#4+1#6	1#4+1#6	1#5+1#7	1#4+1#6	1#4+1#6	1#5+1#7	1#4+1#6	1#4+1#6	1#5+1#7	1#4+1#6	1#4+1#6	1#5+1#7	1#4+1#6	1#4+1#6	
		Int. Spans	1#5+1#7	1#4+1#6	1#4+1#6	1#5+1#7	1#4+1#6	1#4+1#6	1#5+1#7	1#4+1#6	1#4+1#6	1#5+1#7	1#4+1#6	1#4+1#6	1#5+1#7	1#4+1#6	1#4+1#6	1#5+1#7	1#4+1#6	1#4+1#6	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
		1 st Int. Support	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
26	Bottom Reinforcement	End Spans	2#6	1#5+1#7	1#4+1#6	2#6	1#5+1#7	1#4+1#6	2#6	1#5+1#7	1#4+1#6	2#6	1#5+1#7	1#4+1#6	2#6	1#5+1#7	1#4+1#6	2#6	1#5+1#7	1#4+1#6	
		Int. Spans	2#6	1#5+1#7	1#4+1#6	2#6	1#5+1#7	1#4+1#6	2#6	1#5+1#7	1#4+1#6	2#6	1#5+1#7	1#4+1#6	2#6	1#5+1#7	1#4+1#6	2#6	1#5+1#7	1#4+1#6	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
		1 st Int. Support	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
28	Bottom Reinforcement	End Spans	1#6+1#8	1#4+1#6	1#4+1#6	1#6+1#8	1#4+1#6	1#4+1#6	1#6+1#8	1#4+1#6	1#4+1#6	1#6+1#8	1#4+1#6	1#4+1#6	1#6+1#8	1#4+1#6	1#4+1#6	1#6+1#8	1#4+1#6	1#4+1#6	
		Int. Spans	1#6+1#8	1#4+1#6	1#4+1#6	1#6+1#8	1#4+1#6	1#4+1#6	1#6+1#8	1#4+1#6	1#4+1#6	1#6+1#8	1#4+1#6	1#4+1#6	1#6+1#8	1#4+1#6	1#4+1#6	1#6+1#8	1#4+1#6	1#4+1#6	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
		1 st Int. Support	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
30	Bottom Reinforcement	End Spans	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	
		Int. Spans	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	2#7	2#5	2#5	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	
		1 st Int. Support	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	1#4	1#5	1#5	

Notes

- Shaded portion value shows that joists are provide with shear reinforcement w/ #3 rebar single leg @ 5" O.C.
- Blank Cells indicates that the joists are failing in deflection.

9.12 Table L: $f'_c = 4000$ psi, Topping Thickness = 4.5"

General Data:

Unit weight of concrete = 145 pcf

Δ_i LL = 180

Panel Size = 12"

Δ_i TOTAL = 240

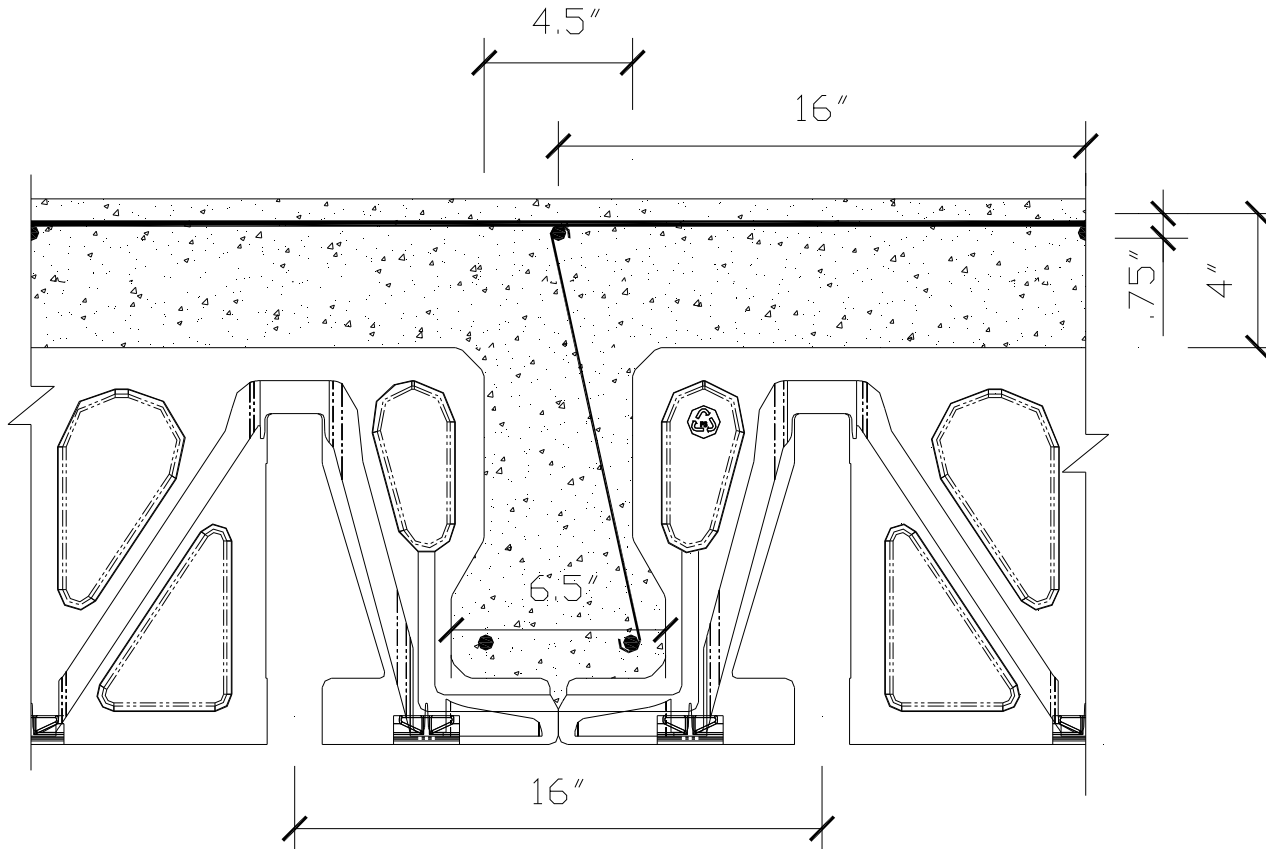
Floor Size: 12" + 4.5"

Rebar strength = 60000 psi

Dead Load Factor = 1.2

2" Standard insulation

Live Load Factor = 1.6



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Dead Load = 10 psf

Bay	No. of Joists	Span	1 - 9' 0" - 15'			1 - 9' 0" - 15'			1 - 9' 0" - 15'			1 - 9' 0" - 15'			1 - 9' 0" - 15'			1 - 9' 0" - 15'			1 - 9' 0" - 15'						
			SP	DF	VS	SP	DF	VS	SP	DF	VS	SP	DF	VS	SP	DF	VS	SP	DF	VS	SP	DF	VS				
1	Full	Full	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'			
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'		
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'
1	Full	Full	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'		
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'
1	Full	Full	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'		
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'
1	Full	Full	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'		
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'
1	Full	Full	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'		
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'
			14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'	14'

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Checked by: Andy / Raj

Date: 12/07/2007

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Dead Load = 15 psf

Span	M	D	1 - 5' 0" - 1'			1 - 5' 0" - 1'			1 - 5' 0" - 1'			1 - 5' 0" - 1'			1 - 5' 0" - 1'			1 - 5' 0" - 1'			1 - 5' 0" - 1'			
			SP	DP	US	SP	DP	US	SP	DP	US	SP	DP	US	SP	DP	US	SP	DP	US	SP	DP	US	
11	Full	Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
17	Full	Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
14	Full	Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
16	Full	Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
18	Full	Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
20	Full	Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
22	Full	Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
24	Full	Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
26	Full	Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
28	Full	Deck	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
			140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140

Notes

- Shaded portion value shows that joists are provide with shear reinforcement w/ #3 rebar single leg @ 5" O.C.
- Blank Cells indicates that the joists are failing in deflection.

Shoring Design Calculation

Maximum allowed span for steel channel sections supporting the flanges, between the joist is obtained from the minimum of spans based on moment, shear, deflection and crippling.

Joist Spacing	=	16"
Deflection Factor, D_F	=	360 & 480
Modulus of Elasticity of Steel, E_S	=	29000 Ksi
Steel Joist Type	=	1000S162-54
Self weight of joist	=	(Area of Joist/ 2 x Unit wt. of concrete)
W_{DJ}	=	(51.9888/2 x 145)/144
	=	26.18 plf
Self weight of topping	=	(16 x topping thickness x Unit wt. of concrete) /144
W_{DT}	=	16 x 2 x 145/144
	=	32.22 plf
Self weight of AmDeck Block	=	1.3 x 16/12
	=	1.73 plf
Total dead load	=	Self weight of joist + Self weight of topping + Self weight of AmDeck Block
	=	26.18 + 32.22 + 1.73
	=	60.13 plf

As per ACI 347-02, Construction load to be taken as 50 psf.

Construction load	=	Joist Spacing x W_{LL} / 12
	=	16 x 50/12
	=	66.67 plf
Self weight of steel joist	=	$W_{DL\ Steel}$
For 1000S162-54 Joist		
Self weight of steel joist, $W_{DL\ Steel}$	=	2.66 plf
Total Load, W	=	Total Dead Load + Live load + Self wt. of steel joist
	=	60.13 + 66.67 + 2.66
	=	129.46 plf

Maximum Allowed span

Based on Allowable Moment

Allowable moment =	M_{Max} from Amvic Steel joist chart
M_{Max}	= $W \times L^2 / 8$
$70.7 \times 1000/12$	= $W \times L^2 / 8$
70.70	= $129.46 \times L^2 / 8$
L	= $\sqrt{70.70 \times 8/129.46}$
	= 19.08 ft

Based on Allowable shear

$$\begin{aligned}
 V_x &= W \times L/2 \\
 2.12 \times 1000 &= 129.46 \times L/2 \\
 L &= 2 \times 2120 / 129.46 \\
 &= 32.75 \text{ ft}
 \end{aligned}$$

Based on Crippling

$$\begin{aligned}
 \text{Web Crippling Load, } P_r &= W \times L / 2 \\
 1.1 \times 10^3 &= 129.46 \times L/2 \\
 L &= 1.1 \times 10^3 \times 2 / 129.46 \\
 &= 16.99 \text{ ft} \\
 \text{Maximum Span of Shoring} &= \text{Minimum of (19.08, 32.75, 14.565 \& 16.99)} \\
 &= 14.50 \text{ ft}
 \end{aligned}$$

Based on Deflection factor

i. Deflection Factor, ADF = L/360

$$\begin{aligned}
 \text{Allowable deflection, ADF} &= L / \text{Deflection factor (D}_F\text{)} \\
 L / 360 &= \frac{5}{384} \times \frac{129.46 \times L^4}{29 \times 10^6 \times \frac{9.31}{144}} \\
 L &= 14.565 \text{ ft}
 \end{aligned}$$

ii. Deflection Factor, ADF= L/480

$$\begin{aligned}
 \text{Allowable deflection, ADF} &= L / \text{Deflection factor (D}_F\text{)} \\
 L / 480 &= \frac{5}{384} \times \frac{129.46 \times L^4}{29 \times 10^6 \times \frac{9.31}{144}} \\
 L &= 13.23 \text{ ft}
 \end{aligned}$$

$$\begin{aligned}
 \text{Maximum Span of Shoring} &= \text{Minimum of (19.08, 32.75, 13.23 \& 16.99)} \\
 &= 13.00 \text{ ft}
 \end{aligned}$$

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9.13 Shoring Span Table

Allowable Deflection factor	L/360			L/480		
	Topping (in)	1000S162-54	1000S162-68	1000S162-97	1000S162-54	1000S162-68
2.0	14.5	15.5	17.5	13.0	14.0	16.0
2.5	14.0	15.0	17.0	12.5	14.0	15.5
3.0	13.5	15.0	17.0	12.5	13.5	15.0
3.5	13.5	14.5	16.5	12.0	13.5	15.0
4.0	13.5	14.5	16.0	12.0	13.0	14.5
4.5	12.5	14.0	16.0	12.0	13.0	14.5

10 Garage Deck Joist Design Criteria

Panel Designation	=	12" Panel section with 10" deep beam
Beam Depth	=	d_w in inches
Topping	=	t_f in inches
Minimum Beam Width, bottom	=	b_w in inches
Average Joist Width	=	b_{wa} in inches
Panel Span, Transverse	=	b in inches
Maximum Span of the Deck	=	L in feet & inches
Number of Span	=	Single (SS) / Double (DS)
Live load acting on the deck	=	w_{LL} in psf
Dead load acting on the deck	=	w_{DL} in psf
Wheel Load	=	P in lb
Distance between Front & Rear Wheel	=	x in feet
Unit weight of concrete	=	γ_c in pcf
Specified compressive strength of concrete	=	f'_c in psi
Yield strength of rebar	=	f_y in psi
Rebar cover, Center of rebar (bottom)	=	c in inches
Rebar cover, Center of rebar (top)	=	d' in inches (take as $t_f/2$)
Allowable Deflection factor, Total	=	$\Delta_{Factor Total}$
Allowable Deflection factor, LL	=	$\Delta_{Factor LL}$

10.1 Assumptions

- i. Design criteria are based on **IBC 2003 + ACI 318-02** codes.
- ii. Modulus of elasticity of rebar is assumed to be 29000 ksi for the design.
- iii. 'Normal weight concrete' is assumed to be used in wall construction and therefore $\lambda = 1.0$ corresponding to 'Normal weight concrete' has been use in design.
- iv. Factored load combination of $1.2DL + 1.6LL$ is used in strength calculation & service load $DL + LL$ is used in deflection calculation.
- v. 'AmDeck floor system' is of type 'Concrete joist construction' as specified in code.
- vi. Vehicle point load is acting at equal distance from both support for the calculation of maximum moment & maximum deflection for Garage joist design.
- vii. One of the vehicle point load is taken @ support & other @ distance "X" from support in shear calculation for garage joist design.
- viii. The distance between vehicle front & rear wheel is taken as 8'-0".
- ix. Point load is assumed to act in middle of top slab for maximum moment calculation.

Dead Load factor = K_{DL}

Live Load factor = K_{LL}

10.2 Garage Slab Design

Since, $L_y / L_x > 2$

Slab is designed as one way.

Assume width of slab	=	b in feet
Self weight of slab	=	W_{slab} in plf
Imposed Dead Load	=	$W_{DL} \times b$ in plf
Imposed Live load	=	$W_{LL} \times b$ in plf
Total un-factored Dead load	=	(Self weight of slab + Imposed Dead Load) in plf
Total un-factored Live load	=	Imposed Live load in plf
Total Factored Load, W_{Slab}	=	$K_{DL} \times (\text{Self weight of slab} + w_{DL}) + K_{LL} \times W_{LL}$
Effective span	=	L_{Slab} in feet
Maximum Moment, M_U	=	Moment due to Wheel Load + Moment due to W_{Slab}
	=	$(K_{LL} \times P) \times b / 4 + W_{Slab} \times b^2 / 12$
		(Since slab is continuous over multiple supports)

Determination of reinforcement

Reinforcement ratio, $\rho = (0.85 \times f'_c / f_y) \times \{1 - [1 - 2 \times M_U / (\phi \times b \times d'^2 \times 0.85 \times f'_c)]^{0.5}\}$

Area of reinforcement required ($A_{S_{req}}$) = $\rho \times b \times d$

Area of rebar = $\pi / 4 \times (\# \text{ of rebar} / 8)^2$ in in^2

Spacing of rebar = (Area of rebar / $A_{S_{required}}$) \times width of slab

Punching Shear check for Garage Slab under Wheel Load

Concentrated load for residential car = P_1 in lb

Length of bearing area = L_1 in inches

Bearing area, A_1 = $L_1 \times L_1$ in sq. inch

Self weight of slab = $A_1 \times t_f \times 145 / (144 \times 12)$

Total Factored Load, P_u = 1.2 DL + 1.6LL

Perimeter of bearing area for two-way shear, b_0 = $\{4 \times (L_1 + d')\}$ in inches

Shear strength of concrete in two-way shear, $\phi_v V_c$ = $[\phi_v \times 4 \times \sqrt{f'_c} \times b_0 \times d']$ in lb

10.3 Garage Deck Joist

10.3.1 Analysis

Section Properties

Cross-section area of Combined Section (A) = As Provided by Amvic (Refer Table below)

Distance of CG from top (CG_{Top}) = As Provided by Amvic (Refer Table below)

Moment of inertia about x-axis (I_{xx}) = As Provided by Amvic (Refer Table below)

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below)

$$\text{Section Modulus about x-axis (S}_{XX}) = I_{XX} / (\text{Max (CG}_{\text{Top}}, (d_w + t_f - \text{CG}_{\text{Top}})))$$

Topping (inch)	Area (in ²)	Perimeter (inch)	I _{xx} (in ⁴)	I _{yy} (in ⁴)	R _x (inch)	R _y (inch)	Cg _{Top} (inch)	Cg _{Bottom} (inch)
2	115.9922	88.9652	1632.1071	5587.8915	3.7511	6.941	3.8451	8.1549
2.5	131.9922	89.9652	1868.2302	6953.2249	3.7622	7.258	3.8487	8.6513
3.0	147.9922	90.9652	2108.2903	8318.5582	3.7744	7.497	3.9056	9.0944
3.5	163.9922	91.9652	2357.9644	9683.8916	3.7919	7.685	4.001	9.4999
4.0	179.9922	92.9652	2621.6218	11049.2249	3.8164	7.835	4.1223	9.8777
4.5	195.9922	93.9652	2902.8583	12414.558	3.8485	7.959	4.2654	10.2346
5.0	211.9922	94.9652	3204.7879	13779.8915	3.8881	8.062	4.4246	10.5754

$$\begin{aligned} \text{Effective depth (d)} &= d_w - c + t_f \\ \text{Self weight of deck (w}_{\text{Self}}) &= w_C \times A / 144 \\ \text{Total Dead Load } W_{\text{DTotal}} &= w_{\text{Self}} + w_{\text{DL}} \times b / 12 \\ \text{Live Load } W_{\text{LL}} &= w_{\text{LL}} \times b / 12 \\ \text{Total Unfactored UDL } W_{\text{P}} &= W_{\text{DTotal}} + W_{\text{LL}} \\ \text{Total factored UDL (W}_{\text{U}}) &= \{K_{\text{DL}} \times W_{\text{DTotal}} + K_{\text{LL}} \times W_{\text{LL}}\} \\ \text{Factored Point Load, } P_{\text{U}} &= K_{\text{LL}} \times P \\ \text{Maximum Shear Force (V}_{\text{U}}) & \\ &= K_{\text{DL}} \times W_{\text{DTotal}} \times L / 2 + \text{Maximum (} K_{\text{LL}} \times W_{\text{LL}} \times L / 2, P_{\text{U}} \times (2 - x / L) \text{)} \quad \text{For (} x < L \text{)} \\ &= K_{\text{DL}} \times W_{\text{DTotal}} \times L / 2 + \text{Maximum (} K_{\text{LL}} \times W_{\text{LL}} \times L / 2, P_{\text{U}} \text{)} \quad \text{For (} x > L \text{)} \end{aligned}$$

Maximum Positive Moment (M_{UP})

$$\begin{aligned} \text{a. For Single Span} & \\ &= (K_{\text{DL}} \times W_{\text{DTotal}} \times L^2 / 8) + \text{Maximum (} K_{\text{LL}} \times W_{\text{LL}} \times L^2 / 8, P_{\text{U}} \times L / 4 \text{)} \quad \text{For (} x \geq L/2 \text{)} \\ &= (K_{\text{DL}} \times W_{\text{DTotal}} \times L^2 / 8) + \text{Maximum (} K_{\text{LL}} \times W_{\text{LL}} \times L^2 / 8, P_{\text{U}} \times (L-x) / 2 \text{)} \quad \text{For (} x < L/2 \text{)} \\ \text{b. For Double Span} & \\ &= (K_{\text{DL}} \times W_{\text{DTotal}} \times L^2 / 14) + \text{Maximum (} K_{\text{LL}} \times W_{\text{LL}} \times L^2 / 8, P_{\text{U}} \times L / 4 \text{)} \quad \text{For (} x \geq L/2 \text{)} \\ &= (K_{\text{DL}} \times W_{\text{DTotal}} \times L^2 / 14) + \text{Maximum (} K_{\text{LL}} \times W_{\text{LL}} \times L^2 / 8, P_{\text{U}} \times (L-x) / 2 \text{)} \quad \text{For (} x < L/2 \text{)} \end{aligned}$$

10.3.2 Design

10.3.2.1 Shear Strength

$$\text{Shear Strength of the section } (\phi V_c) = 1.1 \times 0.75 \times 2 \times (f'_c)^{0.5} \times b_w a \times d$$

If $\phi V_c < V_u$, Provide Single leg stirrup rebar and provide corresponding rebar at top to support stirrups.

{

$$\text{Area of single leg rebar stirrup} = A_v \text{ in}^2$$

$$\text{Spacing of stirrup rebar} = S_s \text{ in}$$

$$\text{Shear strength provided by shear reinforcement } (\phi V_s) = 0.75 \times A_v \times f_y \times d / S_s$$

$$\text{Total Shear strength } (\phi V_N) = \phi V_c + \phi V_s$$

10.3.2.2 Moment Strength

Strength reduction factor (ϕ) = 0.9

β_1 = 0.85 if ($f'c \leq 4000$ psi)
0.80 if ($4000 < f'c \leq 5000$ psi)
0.75 if ($5000 < f'c \leq 6000$ psi)
0.65 if ($6000 < f'c$)

Balanced reinforcement ratio (ρ_t) = $0.319 \times \beta_1 \times f'c / f_y$

Maximum allowed reinforcement ratio (ρ_{Max}) = ρ_t

Minimum reinforcement ratio (ρ_{Min}) = $\text{Max}(3 \times (f'c)^{0.5}, 200) / f_y$

Positive Reinforcement

Reinforcement ratio for +ive moment (ρ_{Pos})

$$= (0.85 \times f'c / f_y) \times \{1 - [1 - 2 \times M_{UP} / (\phi \times b_{wa} \times d^2 \times 0.85 \times f'c)]^{0.5}\}$$

Area of reinforcement required ($A_{S_{Pos}}$ req) = $\rho_{Pos} \times b_{wa} \times d$

$A_{S_{Pos}}$ provided > $A_{S_{Pos}}$ required

Negative Reinforcement (For Span > 1)

Reinforcement ratio for -ive moment (ρ_{Neg})

$$= (0.85 \times f'c / f_y) \times \{1 - [1 - 2 \times M_{UN} / (\phi \times b_{wa} \times d^2 \times 0.85 \times f'c)]^{0.5}\}$$

Area of reinforcement required ($A_{S_{Neg}}$ req) = $\rho_{Neg} \times b_{wa} \times d$

$A_{S_{Neg}}$ provided > $A_{S_{Neg}}$ required

Nominal moment strength

Plain Concrete

Nominal moment strength of the section (ϕM_n) = $0.65 \times 5 (f'c)^{0.5} \times S_{XX}$

Reinforced Concrete

Nominal moment strength of the section (ϕM_n)

$$= \phi A_{S_{Pos}} \text{ provided} \times f_y \times [d - (A_{S_{Pos}} \text{ provided} \times f_y / (0.85 \times f'c \times b))] / 2$$

10.3.2.3 Deflections

Total depth of section (h) = $d_w + t_f$

A_{LP} = $A_{S_{Neg}}$ provided

A_B = $A_{S_{Pos}}$ provided

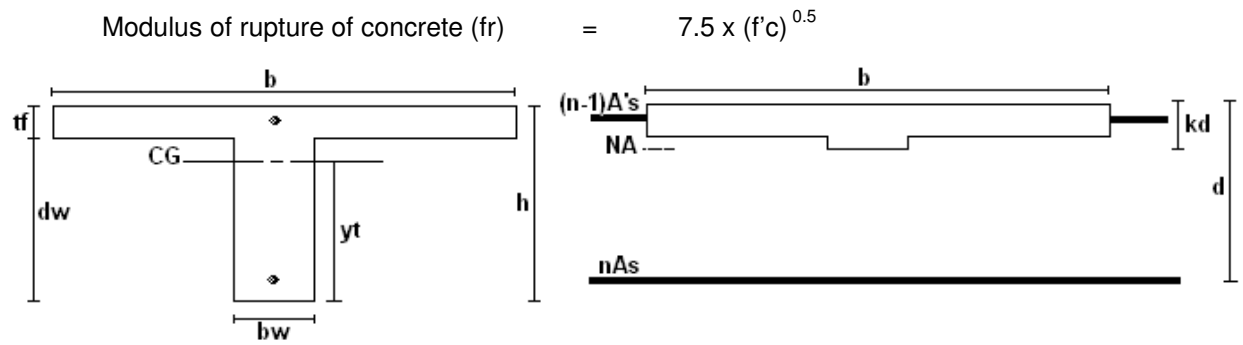
R_{DS} = Diameter of shear rebar

R_{DLP} = Diameter of Single rebar $A_{S_{Neg}}$ provided

Effective depth (d_{LP}) = $d_w + t_f - c - R_{DS} - 0.5R_{DLP}$

Modulus of elasticity of concrete (E_C) = $(\gamma_C)^{1.5} \times (33 \times (f'c)^{0.5})$

Modular ratio (n) = E_S / E_C



Gross Section

Cracked Transformed Section

y_t = C_g Bottom As Provided by Amvic (Refer Table above)

I_g = I_{xx} As Provided by Amvic (Refer Table above)

Cracking Moment (M_{CR}) = $f_r \times I_g / y_t$

C = $bwa / (n \times A_{S\ Pos\ provided})$

f = $t_f \times (b-b_w) / (n \times A_{S\ Pos\ provided})$

r = $(n-1) A_{S\ Neg\ provided} / (n A_{S\ Pos\ provided})$

d' = $h - d_{LP}$

$$kd = \frac{\sqrt{C(2d + t_f \times f + 2rd') + (f + r + 1)^2} - (f + r + 1)}{C}$$

Moment of inertia of cracked section transformed to concrete (I_{cr})

$$= (b - b_w)t_f^3 / 12 + b_w(kd)^3 / 3 + (b - b_w)t_f(kd - t_f / 2)^2 + nA_{Bi}(d - kd)^2 + (n - 1)A_{LPi}(kd - d')^2$$

Service Moment (M_P)

Dead Load moment, M_D = $W_{D\ Total} \times L^2 / 8$

Live Load moment, M_{L1} = $W_{LL} \times L^2 / 8$ (Due to UDL)

Live Load moment, M_{L2} = $P \times L / 4$ ($x \geq L / 2$)

= $P \times (L - x) / 2$ ($x < L / 2$)

Total Live Load Moment, M_L = $M_{L1} + M_{L2}$

Total moment, M_{D+L} = $M_D + M_L$

Sustained Moment, $M_{SUS\ 1}$ = $M_D + 0.5 \times M_{L1}$ *Assuming that 50% of live Load as sustained load*

Sustained Moment, $M_{SUS\ 2}$ = $0.5 \times M_{L2}$ *(Assuming that 50% of live Load as sustained load)*

Effective moment of inertia for deflection computation (I_e)

= I_g if $M_{CR} > M_P$

= Minimum of $\{[(M_{CR} / M_P)^3 I_g + [1 - (M_{CR} / M_P)^3] I_{CR}\}$ and I_g if $M_{CR} \leq M_P$

10.3.2.4 Short Term Deflection

For Uniformly Distributed Load

$$\text{Mid-span deflection is } \Delta_I = K (5/48) M_P \times L^2 / (E_c \times I_e)$$

For Point Load

$$\begin{aligned} \text{Mid-span deflection } \Delta_{ip} &= \{P \times L^3\} / (48 \times E_c \times I_e) && (x \geq L/2) \\ &= \{P \times (L - x)/2\} \times \{3 \times L^2 - 4 \times ((L - x)/2)^2\} / (24 \times E_c \times I_e) && (x < L/2) \end{aligned}$$

Where,

$$K = 1.0 \quad \text{for Simple Beam}$$

$$\Delta_{iD} = K (5/48) M_D \times L^2 / (E_c \times I_e)$$

$$\begin{aligned} \Delta_{i \text{ Total}} &= K (5/48) M_{(D+L) \text{ UDL}} \times L^2 / (E_c \times I_e) \\ &+ \{P \times (L - x)/2\} \times \{3 \times L^2 - 4 \times ((L - x)/2)^2\} / (24 \times E_c \times I_e) \quad (x < L/2) \end{aligned}$$

$$= K (5/48) M_{(D+L) \text{ UDL}} \times L^2 / (E_c \times I_e) + \{P \times L^3\} / (48 \times E_c \times I_e) \quad (x \geq L/2)$$

$$\begin{aligned} \Delta_{i \text{ SUS}} &= K (5/48) M_{\text{SUS}1} \times L^2 / (E_c \times I_e) \\ &+ \{0.5 \times P \times (L - x)/2\} \times \{3 \times L^2 - 4 \times ((L - x)/2)^2\} / (24 \times E_c \times I_e) \quad (x < L/2) \end{aligned}$$

$$= K (5/48) M_{\text{SUS}1} \times L^2 / (E_c \times I_e) + \{0.5 \times P \times L^3\} / (48 \times E_c \times I_e) \quad (x \geq L/2)$$

$$\Delta_{i \text{ LL}} = \Delta_{i \text{ Total}} - \Delta_{i \text{ DL}}$$

Allowable Short Term Deflections

$$\Delta_{i \text{ Allow LL}} = (L \times 12) / (180 \text{ or } 360)$$

10.3.2.5 Long Term Deflection

$$\Delta_{(CP+SH)} = \lambda \times \Delta_{i \text{ SUS}}$$

Where

$$\lambda = \xi / (1+50\rho')$$

$$\rho' = \text{Area of compression steel (A')} / (b \times w \times d)$$

$$\xi = \text{Time- dependent factor}$$

$$= 2.0 \quad \text{5 years and more Sustained load duration}$$

$$= 1.4 \quad \text{12 months}$$

$$= 1.2 \quad \text{6 months}$$

$$= 1.0 \quad \text{3 months.}$$

$$\Delta_{LT} = \Delta_{(CP+SH)} + \Delta_{i \text{ LL}}$$

Allowable Long Term Deflection

$$\Delta_{i \text{ Allow LL}} = (L \times 12) / 240 \text{ or } 480$$

11 Slab Reinforcement Design Criteria

11.1 Transverse Reinforcement

$$L_{\text{Slab}} = b/12$$

$$M_{u \text{ Slab}} = P_u \times L_{\text{Slab}}^2 / 12$$

$$\text{Balanced reinforcement ratio } (\rho_t) = 0.319 \times \beta_1 \times f'_c / f_y \quad (\text{Per Section 7.1 of Notes on ACI 318-02})$$

$$\text{Maximum allowed reinforcement ratio } (\rho_{\text{Max}}) = \rho_t$$

$$\text{Minimum reinforcement ratio } (\rho_{\text{Min}}) = \text{Max } (3 \times (f'_c)^{0.5}, 200) / f_y \quad (\text{Per Section 10.5.1 ACI 318-02})$$

$$\text{Reinforcement ratio for +ive moment } (\rho_{\text{Pos}})$$

$$= (0.85 \times f'_c / f_y) \times \{1 - [1 - 2 \times M_{\text{UP}} / (\phi \times b_w \times t_f / 2^2 \times 0.85 \times f'_c)]^{0.5}\}$$

$$\text{Area of reinforcement required } (A_{S \text{ Pos req}}) = \rho_{\text{Pos}} \times 12 \times t_f / 2$$

$$\text{Area of reinforcement required } (A_{S \text{ Pos req}}) \text{ (Minimum)} = \rho_{\text{Min}} \times 12 \times t_f / 2$$

$$\text{Area of reinforcement required } (A_{S \text{ Pos req}}) \text{ (Maximum)} = \rho_{\text{Max}} \times 12 \times t_f / 2$$

$$\text{If } A_{S \text{ Pos req}} \text{ (Minimum)} > A_{S \text{ Pos req}}$$

$$\text{Then Provided Area of Steel} = \text{Minimum of } A_{S \text{ Pos req}} \text{ (Minimum) or } 1.33 \times A_{S \text{ Pos req}}$$

$$\text{If } A_{S \text{ Pos req}} \text{ (Minimum)} \leq A_{S \text{ Pos req}}$$

$$\text{Then Provided Area of Steel} = A_{S \text{ Pos req}}$$

$$\text{Minimum Spacing, } S_{\text{Calculated}} = (A_{\text{rebar}} / \text{Area of Steel Provided}) \times 12$$

However per section 7.12 of ACI 318-02, minimum spacing will be lesser of following three

- (1) $S_{\text{Calculated}}$
- (2) 18" O.C.
- (3) $5 \times t_f$ (t_f is thickness of slab)

11.2 Longitudinal Reinforcement

Minimum Longitudinal reinforcement as per section 7.12 of ACI 318-02 to be calculated by following equation.

$$\text{For Grade 60 rebar, } A_s \text{ Minimum} = 0.0018 \times \text{Cross sectional Area}$$

$$\text{Spacing for } A_s \text{ Minimum, } S_{\text{Calculated}} = (A_{\text{rebar}} / \text{Area of Steel Provided}) \times 12$$

However per section 7.12 of ACI 318-02, minimum spacing will be lesser of following three

- (1) $S_{\text{Calculated}}$
- (2) 18" O.C.
- (3) $5 \times t_f$ (t_f is thickness of slab)

12 Garage Deck Joist Design Calculation

(12" Panel Size With 10" Deep Joist @ 32" O.C. And 4" Topping Slab)

Single Span beam

Inputs

Panel Designation	=	12" Panel section with 10" deep beam
Beam Depth (d_w)	=	10"
Topping (t_f)	=	4"
Minimum Beam Width, bottom (b_w)	=	6.5"
Average Joist Width (b_{wa})	=	5.2"
Panel Span, Transverse (b)	=	32"
Maximum Span of the Deck (L)	=	15'-0"
Number of Span	=	Single
Live load acting on the deck (w_{LL})	=	50 psf
Dead load acting on the deck (w_{DL})	=	10 psf
Wheel Load (P)	=	3000 lb
Distance between Front & Rear Wheel (x)	=	8'-0"
Unit weight of concrete (γ_c)	=	145 pcf
Specified compressive strength of concrete (f'_c)	=	3500 psi
Yield strength of rebar (f_y)	=	60000 psi
Rebar cover, Center of bottom rebar (c)	=	1.25"
Rebar cover, clear of top rebar (d')	=	2" ($=t_f/2$)
Allowable Deflection factor, Total ($\Delta_{Factor LL}$)	=	180 or 360 (Short Term)
Allowable Deflection factor, Total ($\Delta_{Factor LL}$)	=	240 or 480 (Long Term)
Dead Load factor (K_{DL})	=	1.2
Live Load factor (K_{LL})	=	1.6

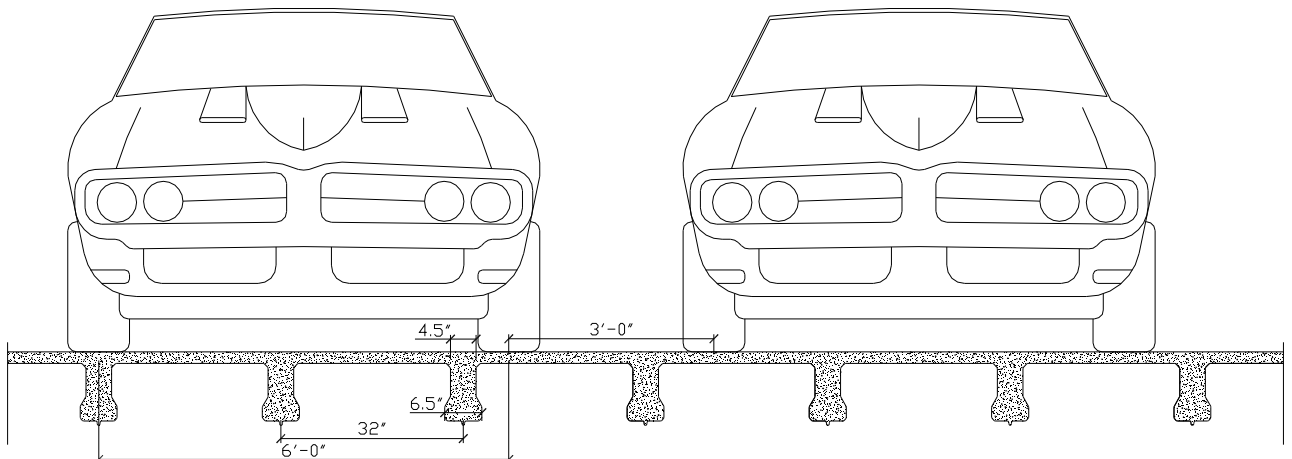
ence Provide #4 Rebar @ 16" O.C. in Longitudinal direction.

12.1 Garage Joist Design

12.1.1 Analysis

Section Properties

Cross-section area A	=	179.9888 in ²
Distance of CG from top (CG_{Top})	=	4.1223 in from top
Moment of inertia about x-axis (I_{xx})	=	2621.6 in ⁴
Section Modulus about x-axis (S_{xx})	=	2621.6 / {Max [4.1223, (10 + 4 - 4.1223)]}
	=	265.4 in ³
Effective depth (d)	=	$d_w - c + t_f$
	=	10 - 1.25 + 4
	=	12.75"
Self weight of deck (w_{Self})	=	$w_C \times A_{Gross}$
	=	145 x 179.9888/144
	=	181.239 plf
Total Dead Load W_{DTotal}	=	181.239 + 10 x 32/12
	=	207.91 plf
Live Load W_{LL}	=	50 x 32/12
	=	133.33 plf
Total Unfactored UDL (W_P)	=	$W_{DTotal} + W_{LL}$
	=	207.91 + 133.33
	=	341.24 plf
Total factored UDL (W_U)	=	{ $K_{DL} \times W_{DTotal} + K_{LL} \times W_{LL}$ }
	=	1.2 x 207.91 + 1.6 x 133.33
	=	462.82 plf



$$\begin{aligned} \text{Factored Point load (P}_U) &= K_{LL} \times P \\ &= 1.6 \times 3000 \\ &= 4800 \text{ lb} \end{aligned}$$

$$\begin{aligned} \text{Maximum Shear Force (V}_U) &= K_{DL} \times W_{D \text{ Total}} \times L / 2 + \text{Maximum (K}_{LL} \times W_{LL} \times L / 2, P_U \times (2 - x / L)) \quad \text{For (x < L)} \\ &= 1.4 \times 207.91 \times 15 / 2 + \text{Maximum (1.6 \times 133.33 \times 15 / 2, 4800 \times (2 - 8 / 15))} \\ &= 9223.01 \text{ lb.} \end{aligned}$$

$$\begin{aligned} \text{Maximum Positive Moment (M}_{UP}) &= (K_{DL} \times W_{D \text{ Total}} \times L^2 / 8) + \text{Maximum (K}_{LL} \times W_{LL} \times L^2 / 8, P_U \times L / 4) \quad \text{For (x \ge L/2)} \\ &= (1.4 \times 207.91 \times 15^2 / 8) + \text{Maximum (1.6 \times 133.33 \times 15^2 / 8, 4800 \times 15 / 4)} \\ &= 23530.41 \text{ ft-lb} = 282364.9 \text{ in-lb.} \end{aligned}$$

12.1.2 Shear Strength

$$\begin{aligned} \text{Shear Strength of the section (}\phi V_c) &= 1.1 \times 0.75 \times 2 \times (f'c)^{0.5} \times b_{wa} \times d \\ &= 1.1 \times 0.75 \times 2 \times (3500)^{0.5} \times 5.2 \times 12.75 \\ &= \mathbf{6471.895 \text{ lb.} < V_U (= 9223.01 \text{ lb.) (Not OK)} \end{aligned}$$

Hence Shear Stirrups provided

$$\begin{aligned} \text{Area of single leg of \#3 rebar} &= \pi/4 \times (3/8)^2 \\ &= 0.110 \text{ in}^2 \end{aligned}$$

$$\text{Spacing of stirrup rebar} = 5 \text{ in}$$

$$\begin{aligned} \text{Shear strength provided by shear reinforcement (}\phi V_s) &= 0.75 \times 0.11 \times 60000 \times 12.75 / 5 \\ &= 12622.5 \text{ lb} \end{aligned}$$

$$\begin{aligned} \text{Total Shear strength (}\phi V_N) &= \phi V_c + \phi V_s \\ &= 6471.895 + 12622.5 \\ &= \mathbf{19094.4 \text{ lb} > V_U (= 9223.01 \text{ lb.) (OK)} \end{aligned}$$

12.1.3 Moment Strength

$$\begin{aligned} \text{Strength reduction factor (}\phi) &= 0.9 \\ \beta_1 &= 0.85 \quad \text{if (f'c \le 4000 psi)} \\ &= 0.80 \quad \text{if (4000 < f'c \le 5000 psi)} \\ &= 0.75 \quad \text{if (5000 < f'c \le 6000 psi)} \\ &= 0.65 \quad \text{if (6000 < f'c)} \\ \beta_1 &= 0.85 \quad \text{since (f'c \le 4000 psi)} \end{aligned}$$

$$\begin{aligned} \text{Tension controlled reinforcement ratio (}\rho_b) &= 0.319 \times 0.85 \times 3500 / 60000 \\ &= 0.0158 \end{aligned}$$

$$\begin{aligned}
 \text{Maximum allowed reinforcement ratio } (\rho_{\text{Max}}) &= \rho_t \\
 &= 0.0158 \\
 \text{Minimum reinforcement ratio } (\rho_{\text{Min}}) &= \text{Max } (3 \times (f'c)^{0.5}, 200) / f_y \\
 &= \text{Max } (3 \times (3500)^{0.5}, 200) / 60000 \\
 &= \text{Max } (177.5, 200) / 60000 \\
 &= 200 / 60000 \\
 &= 0.0033
 \end{aligned}$$

Positive Reinforcement

$$\begin{aligned}
 \text{Reinforcement ratio for +ive moment } (\rho_{\text{Pos}}) &= (0.85 \times f'c / f_y) \times \{1 - [1 - 2 \times M_{UP} / (\phi \times b_{wa} \times d^2 \times 0.85 \times f'c)]^{0.5}\} \\
 &= (0.85 \times 3500 / 60000) \{1 - [1 - 2 \times 282364.9 / (0.9 \times 5.2 \times 12.75^2 \times 0.85 \times 3500)]^{0.5}\} \\
 &= 0.006629 > (\rho_{\text{Min}} = 0.0033) \\
 &< (\rho_{\text{Max}} = 0.0158) \quad \text{OK}
 \end{aligned}$$

$$\begin{aligned}
 \text{Area of reinforcement required } (A_S \text{ req}) &= \rho_{\text{Pos}} \times b_{wa} \times d \\
 &= 0.006629 \times 5.2 \times 12.75 \\
 &= 0.4395 \text{ in}^2
 \end{aligned}$$

$$A_S \text{ provided} = 2 \#5 \text{ (Area} = 0.6136 \text{ in}^2 > 0.4395 \text{ in}^2) \quad \text{OK}$$

Nominal moment strength**Plain Concrete**

$$\begin{aligned}
 \text{Nominal moment strength of the section } (\phi M_n) &= 0.65 \times 5 \times (f'c)^{0.5} \times S_{XX} \\
 &= 0.65 \times 5 \times (3500)^{0.5} \times 265.4 \\
 &= 51029.15 \text{ in-lb.}
 \end{aligned}$$

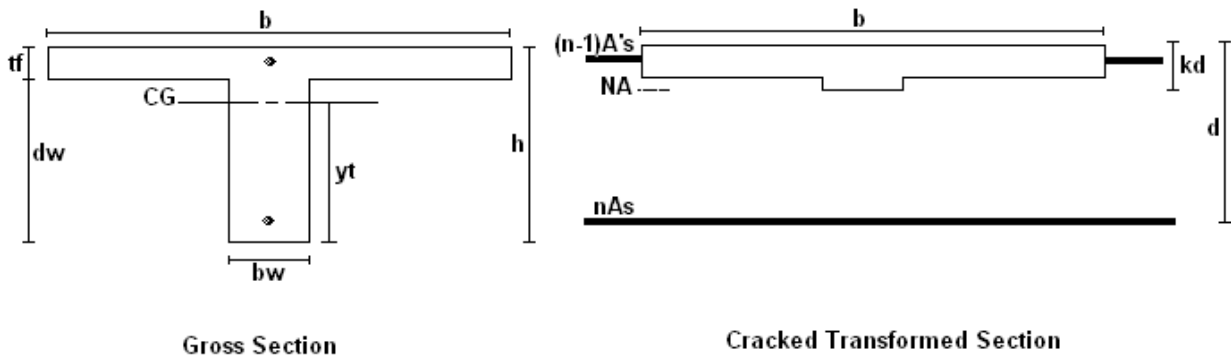
Reinforced Concrete

Nominal moment strength of the section (ϕMn)

$$\begin{aligned}
 &= \phi A_{S \text{ Pos provided}} \times f_y \times [d - (A_{S \text{ Pos provided}} \times f_y / (0.85 \times f'_c \times b))/2] \\
 &= 0.9 \times 0.6136 \times 60000 \times [12.75 - (0.6136 \times 60000 / (0.85 \times 3500 \times 32))/2] \\
 &= \mathbf{416056 \text{ in-lb.}}
 \end{aligned}$$

12.1.4 Deflections

$$\begin{aligned}
 \text{Dead Load moment, } M_D &= 207.91 \times 15^2 / 8 \times 12 \\
 &= 70170 \text{ lb-in} \\
 \text{Live Load (UDL) moment, } M_{L1} &= 133.33 \times 15^2 / 8 \times 12 \\
 &= 45000 \text{ lb-in} \\
 \text{Live Load (Point) moment, } M_{L2} &= 3000 \times 15 / 4 \times 12 \quad \text{since } (x > L/2) \\
 &= 135000 \text{ lb-in} \\
 \text{Total moment, } M_{D+L \text{ (UDL)}} &= 70170 + 45000 \\
 &= 115171 \text{ lb-in} \\
 \text{Sustained Moment, } M_{SUS1} &= M_D + 0.5 \times M_L \quad (\text{Assume that 50\% Load as sustained}) \\
 &= 70170 + 0.5 \times 45000 \\
 &= 92670 \text{ lb-in} \\
 \text{Sustained Moment, } M_{SUS2} &= 0.5 \times 135000 \quad (\text{Assume that 50\% Load as sustained}) \\
 &= 67500 \text{ lb-in} \\
 \text{Total depth of section (h)} &= d_w + t_f \\
 &= 10 + 4 \\
 &= 14'' \\
 \text{Modulus of elasticity of concrete (} E_C \text{)} &= (\gamma_C)^{1.5} \times (33 \times (f'_c)^{0.5}) \\
 &= (145)^{1.5} \times (33 \times (3500)^{0.5}) \\
 &= 3408788 \text{ psi} \\
 \text{Modulus of elasticity of steel (} E_S \text{)} &= 29000000 \text{ psi} \\
 \text{Modular ratio (n)} &= E_S / E_C \\
 &= 29000000 / 3408788 \\
 &= 8.51 \\
 \text{Modulus of rupture of concrete (} f_r \text{)} &= 7.5 \times (f'_c)^{0.5} \\
 &= 7.5 \times (3500)^{0.5} \\
 &= 443.7 \text{ psi}
 \end{aligned}$$



$$y_t = 9.877'' \text{ (As Provided by Amvic)}$$

$$I_g = 2621.6218 \text{ in}^4 \text{ (As Provided by Amvic)}$$

$$\begin{aligned} \text{Cracking Moment (M}_{CR}) &= f_r \times I_g / y_t \\ &= 443.7 \times 2621.6218 / 9.877 \\ &= 108083.64 \text{ in-lb.} \end{aligned}$$

$$\begin{aligned} r &= (n-1) A'_s / (n \times A_s \text{ provided}) \\ &= (8.51-1) \times 0.2613 / (8.51 \times 0.6136) \quad \text{Use } (\pi/4) (4/8)^2 \times (16/12) = 0.2613 \\ &= 0.3758 \end{aligned}$$

$$\begin{aligned} C &= b_{wa} / (n \times A_s \text{ provided}) \\ &= 5.2 / (8.51 \times 0.6136) \\ &= 0.9958 \end{aligned}$$

$$\begin{aligned} f &= t_f \times (b-b_{wa}) / (n \times A_s \text{ provided}) \\ &= 4 \times (32 - 5.2) / (8.51 \times 0.6136) \\ &= 20.5295 \end{aligned}$$

$$\begin{aligned} kd &= \frac{\sqrt{C(2d + t_f \times f) + 2rd'} + (f + r + 1)^2 - (f + r + 1)}{C} \\ &= \frac{[\{0.99 \times (2 \times 12.75 + 4 \times 20.5295 + 2 \times 0.3758 \times 2) + (1+20.5295 + 0.3758)^2\}^{0.5} - (1+20.5295 + 0.3758)]}{0.9958} \\ &= 2.351 \end{aligned}$$

Moment of inertia of cracked section transformed to concrete (Icr)

$$\begin{aligned} &= (b - b_w) t_f^3 / 12 + b_w (kd)^3 / 3 + (b - b_w) t_f (kd - t_f / 2)^2 + n A_{Bi} (d - kd)^2 + (n - 1) A_{Lpi} (kd - d')^2 \\ &= (32 - 5.2) \times 4^3 / 12 + 5.2 \times (2.351)^3 / 3 + (32 - 5.2) (4) (2.351 - 4/2)^2 + 8.51 (0.6136) \\ &\quad (12.75 - 2.351)^2 + (8.51 - 1) (0.196) (2.351 - 2)^2 \\ &= 743.519 \text{ in}^4 \end{aligned}$$

Effective moment of inertia for deflection computation (Ie)

A. Under Dead Load

$$M_{cr} / M_d = 108083.64 / 70170$$

$$= 1.54$$

Hence $(I_e)_d = I_g$

B. Under Sustained Load

$$\begin{aligned} M_{cr} / M_{SUS} &= 108083.64 / (92670 + 67500) \\ &= 0.674 \\ \text{Hence } (I_e)_d &= \text{Minimum of } [(M_{CR} / M_P)^3 I_g + [1 - (M_{CR} / M_P)^3] I_{CR}] \text{ and } I_g \\ &= \text{Min } \{[(108083.64 / 160170)^3 \times 2621.6218 + [1 - (108083.64 / 160170)^3] \times 743.519\} \text{ and } 2621.6218] \\ &= \text{Min } \{1320.625, 2621.6218\} \\ &= 1320.625 \text{ in}^4 \end{aligned}$$

C. Under Dead + Live Load

$$\begin{aligned} M_{cr} / M_{D+L} &= 108083.64 / (115171 + 135000) \\ &= 0.432 \\ \text{Hence } (I_e)_d &= \text{Minimum of } [(M_{CR} / M_P)^3 I_g + [1 - (M_{CR} / M_P)^3] I_{CR}] \text{ and } I_g \\ &= \text{Min } \{[(108083.64 / 250171)^3 \times 2621.6218 + [1 - (108083.64 / 250171)^3] \times 743.519\} \text{ and } 2621.6218] \\ &= \text{Min } \{894.9757, 2621.6218\} \\ &= 894.9757 \text{ in}^4 \end{aligned}$$

12.1.4.1 Short Term Deflection

For Uniformly Distributed Load

$$\text{Mid-span deflection is } \Delta I = K (5/48) MP \times L^2 / (Ec \times I_e)$$

For Point Load

$$\begin{aligned} \text{Mid-span deflection } \Delta_{ip} &= \{2 \times P \times (L - x)/2\} \times \{3 \times L^2 - 4 \times ((L - x)/2)^2\} / (24 \times Ec \times I_e) \quad (x < L/2) \\ &= \{2 \times P \times L^3\} / (48 \times Ec \times I_e) \quad (x \geq L/2) \end{aligned}$$

Where,

K = 1.0 for Simple Beam

$$\begin{aligned} \Delta_{iD} &= K (5/48) M_D \times L^2 / (Ec \times I_e) \\ &= 1.0 \times (5/48) \times 70170 \times (15 \times 12)^2 / (3408788 \times 2621.6218) \\ &= 0.02650'' \\ \Delta_{iSUS} &= K (5/48) M_{SUS1} \times L^2 / (Ec \times I_e) + \{0.5 \times P \times L^3\} / (48 \times Ec \times I_e) \\ &= 1.0 \times (5/48) \times 92670 \times (15 \times 12)^2 / (3408788 \times 1320.625) + \{0.5 \times 3000 \times (15 \times 12)^3\} / \{48 \times 3408788 \times 1320.625\} \\ &= 0.10996'' \\ \Delta_{iTotal} &= K (5/48) M_{(D+L)UDI} \times L^2 / (Ec \times I_e) + \{P \times L^3\} / (48 \times Ec \times I_e) \end{aligned}$$

$$\begin{aligned}
 &= 1.0 \times (5/48) \times 115171 \times (15 \times 12)^2 / (3408788 \times 894.9757) + \{3000 \times (15 \times 12)^3\} / \\
 &\quad \{48 \times 3408788 \times 894.9757\} \\
 &= \mathbf{0.2468''} \\
 \Delta_{i \text{ LL}} &= \Delta_{i \text{ Total}} - \Delta_{i \text{ DL}} \\
 &= 0.2468 - 0.10996 \\
 &= \mathbf{0.13684''}
 \end{aligned}$$

Allowable Short Term Deflections

For $\Delta_{\text{Factor LL}} = 180$

$$\begin{aligned}
 \Delta_{i \text{ Allow LL}} &= (L \times 12) / \Delta_{\text{Factor LL}} \\
 &= (15 \times 12) / 180 \\
 &= \mathbf{1.000''} \\
 &> \Delta_{i \text{ LL}} = \mathbf{0.13684''} \text{ (OK)}
 \end{aligned}$$

For $\Delta_{\text{Factor LL}} = 360$

$$\begin{aligned}
 \Delta_{i \text{ Allow LL}} &= (L \times 12) / \Delta_{\text{Factor LL}} \\
 &= (15 \times 12) / 360 \\
 &= \mathbf{0.5000''} \\
 &> \Delta_{i \text{ LL}} = \mathbf{0.13684''} \text{ (OK)}
 \end{aligned}$$

For $\Delta_{\text{Factor Total}} = 240$

$$\begin{aligned}
 \Delta_{i \text{ Allow Total}} &= (L \times 12) / \Delta_{\text{Factor Total}} \\
 &= (15 \times 12) / 240 \\
 &= \mathbf{0.75''} \\
 &> \Delta_{i \text{ Total}} = \mathbf{0.13684''} \text{ (OK)}
 \end{aligned}$$

For $\Delta_{\text{Factor Total}} = 480$

$$\begin{aligned}
 \Delta_{i \text{ Allow Total}} &= (L \times 12) / \Delta_{\text{Factor Total}} \\
 &= (15 \times 12) / 480 \\
 &= \mathbf{0.3750''} \\
 &> \Delta_{i \text{ Total}} = \mathbf{0.13684''} \text{ (OK)}
 \end{aligned}$$

12.1.4.2 Long term Deflection

- i. Sustained load duration of 3 Months

$$\begin{aligned}
 \lambda &= \xi / (1 + 50 \times p') \\
 p' &= A'_s / bwa \times d \\
 &= 0.196 / (5.17 \times 12.75) \\
 &= 2.973 \times 10^{-3} \\
 \lambda &= 1.0 / (1 + 2.973 \times 10^{-3}) \\
 &= 0.997 \\
 \Delta_{(CP+SH)} &= \lambda \times \Delta_{i \text{ SUS}}
 \end{aligned}$$

$$\begin{aligned}
 &= 0.997 \times 0.10996 \\
 &= 0.1096 \text{ in} \\
 \Delta_{(CP+SH)} + \Delta_{iLL} &= 0.1096 + 0.13684 \\
 &= 0.246 \text{ in}
 \end{aligned}$$

Allowable Deflections

$$\begin{aligned}
 \Delta_{i \text{ Allow}} &= (L \times 12) / \Delta_{\text{Factor}} \\
 &= (15 \times 12) / 240 \\
 &= \mathbf{0.75''} \\
 &> \mathbf{0.246'' \text{ (OK)}}
 \end{aligned}$$

ii. Sustained load duration of 5 years & more

$$\begin{aligned}
 \text{Sustained Moment, } M_{\text{SUS } 1} &= M_D + 0.3 \times M_L \quad (\text{Assume that 30\% Load as sustained}) \\
 &= 70170 + 0.3 \times 45000 \\
 &= 83670 \text{ lb-in} \\
 \text{Sustained Moment, } M_{\text{SUS } 2} &= 0.3 \times 135000 \quad (\text{Assume that 30\% Load as sustained}) \\
 &= 40500 \text{ lb-in}
 \end{aligned}$$

Under Sustained Load

$$\begin{aligned}
 M_{cr} / M_{\text{SUS}} &= 108083.64 / (83670 + 40500) \\
 &= 0.87
 \end{aligned}$$

$$\begin{aligned}
 \text{Hence } (I_e)_d &= \text{Minimum of } \{[(M_{CR} / M_P)^3 I_g + [1 - (M_{CR} / M_P)^3] I_{CR}] \text{ and } I_g\} \\
 &= \text{Min } \{[(108083.64 / 124170)^3 \times 2621.6218 + [1 - (108083.64 / 124170)^3] \times 743.519\} \text{ and } 2621.6218\} \\
 &= \text{Min } \{1982.17, 2621.6218\} \\
 &= 1982.17 \text{ in}^4
 \end{aligned}$$

$$\begin{aligned}
 \Delta_{i \text{ SUS}} &= K (5/48) M_{\text{SUS } 1} \times L^2 / (E_c \times I_e) + \{0.3 \times P \times L^3\} / (48 \times E_c \times I_e) \\
 &= 1.0 \times (5/48) \times 83670 \times (15 \times 12)^2 / (3408788 \times 1982.17) + \{0.3 \times 3000 \times (15 \times 12)^3\} / \{48 \times 3408788 \times 1982.17\} \\
 &= 0.05797
 \end{aligned}$$

$$\begin{aligned}
 \lambda &= \xi / (1 + 50 \times p') \\
 p' &= A'_s / bwa \times d \\
 &= 0.196 / (5.17 \times 12.75) \\
 &= 2.973 \times 10^{-3} \\
 &= 2.0 / (1 + 2.973 \times 10^{-3}) \\
 &= 1.994
 \end{aligned}$$

$$\begin{aligned}
 \Delta_{(CP+SH)} &= \lambda \times \Delta_{i \text{ SUS}} \\
 &= 1.994 \times 0.05797 \\
 &= 0.1156 \text{ in}
 \end{aligned}$$

$$\Delta_{(CP+SH)} + \Delta_{iLL} = 0.1156 + 0.13684$$

$$= 0.2524 \text{ in}$$

Allowable Deflections

For $\Delta_{\text{Factor}} = 240$

$$\begin{aligned} \Delta_{i \text{ Allow}} &= (L \times 12) / \Delta_{\text{Factor}} \\ &= (15 \times 12) / 240 \\ &= \mathbf{0.75''} \\ &> \mathbf{0.2524'' \text{ (OK)}} \end{aligned}$$

For $\Delta_{\text{Factor}} = 480$

$$\begin{aligned} \Delta_{i \text{ Allow}} &= (L \times 12) / \Delta_{\text{Factor}} \\ &= (15 \times 12) / 480 \\ &= \mathbf{0.375''} \\ &> \mathbf{0.2524'' \text{ (OK)}} \end{aligned}$$

12.1.5 Calculation for Transverse Slab Reinforcement

Consider 12" width of slab,

$$\begin{aligned} L_{\text{Slab}} &= 27.5 / 12 \\ &= 2.29 \text{ ft} \end{aligned}$$

$$\begin{aligned} \text{Self weight of deck} &= 145 \times (4 / 12) \times 1 \\ &= 48.33 \text{ plf} \\ \text{Total factored load, } P_U &= 1.2 \times 10 \times 12 / 12 + 1.2 \times 48.33 + 1.6 \times 40 \times 12 / 12 \\ &= 133.9 \text{ plf} \\ \text{Total factored point load} &= 1.6 \times 3000 \\ &= 4800 \text{ lb} \\ \text{Maximum Moment} &= 133.9 \times 2.29^2 / 12 + 4800 \times 2.29 / 4 \\ &= 2806.5 \text{ ft-lb} \\ &= 33678 \text{ in-lb} \end{aligned}$$

$$\begin{aligned} \text{Tension controlled reinforcement ratio } (\rho_t) &= 0.319 \times 0.85 \times 3500 / 60000 \\ &= 0.0158 \end{aligned}$$

$$\begin{aligned} \text{Maximum allowed reinforcement ratio } (\rho_{\text{Max}}) &= \rho_t \\ &= 0.0158 \end{aligned}$$

$$\begin{aligned} \text{Minimum reinforcement ratio } (\rho_{\text{Min}}) &= \text{Max } (3 \times (f'c)^{0.5}, 200) / f_y \\ &= \text{Max } (3 \times (3500)^{0.5}, 200) / 60000 \\ &= \text{Max } (177.5, 200) / 60000 \\ &= 200 / 60000 \\ &= 0.0033 \end{aligned}$$

Reinforcement ratio for +ive moment (ρ_{Pos})

$$\begin{aligned} &= (0.85 \times f'c / f_y) \times \{1 - [1 - 2 \times M_{UP} / (\phi \times b_w \times t_f / 2^2 \times 0.85 \times f'c)]^{0.5}\} \\ &= 0.0159 \\ &= 0.0159 > (\rho_{\text{Min}} = 0.0033) \\ &= 0.0159 > (\rho_{\text{Max}} = 0.0158) \end{aligned}$$

Consulting Engineers, Corp

Project: AmDeck Design Guide

Client: Amvic, Inc.

Prepared by: Kapil

Checked by: Andy / Raj

Date: 12/07/2007

Date: 12/07/2007

$$\begin{aligned}\text{Area of Reinforcement Required} &= 0.0158 \times 12 \times 4/2 \\ &= 0.3792 \text{ in}^2\end{aligned}$$

$$\text{Rebar Used} = \#4 \text{ rebar}$$

$$\text{Area of Rebar} = 0.1963 \text{ in}^2$$

$$\begin{aligned}\text{Spacing} &= (0.1963 / 0.3792) \times 12 \\ &= 6.29 \text{ in}\end{aligned}$$

Per Section 7.12 of ACI-318-02 Spacing of rebar will be Minimum of the following three

- (1) Calculated spacing as above = 6.29 in
- (2) 5 times of thickness of slab = $5 \times 4 = 20$ in
- (3) 18 in

Provide #4 rebar @ 6" O.C.

12.1.6 Calculation for Longitudinal Slab Reinforcement

Consider 12" width of slab,

$$\begin{aligned}\text{Per Section 7.12 of ACI-318-02 Minimum reinforcement} &= 0.0018 \times \text{area of cross section} \\ &= 0.0018 \times 4 \times 12 \\ &= 0.0864 \text{ in}\end{aligned}$$

$$\begin{aligned}\text{Spacing} &= (0.1963 / 0.0864) \times 12 \\ &= 27.26 \text{ in}\end{aligned}$$

Per Section 7.12 of ACI-318-02 Spacing of rebar will be Minimum of the following three

- (1) Calculated spacing as above = 27.26 in
- (2) 5 times of thickness of slab = $5 \times 4 = 20$ in
- (3) 18 in

Provide #4 rebar @ 18" O.C.

Punching Shear check for Garage Slab under Wheel Load

$$\text{Concentrated load for residential car} = 3000 \text{ lb}$$

$$\text{Length of bearing area, } L = 4.5 \text{ in}$$

$$\begin{aligned}\text{Self weight of 4" thick slab} &= (4.5 \times 4.5/144) \times (4/12) \times 145 \\ &= 6.797 \text{ lb}\end{aligned}$$

$$\begin{aligned}\text{Total Factored Load, } P_u &= 1.2 \text{ DL} + 1.6 \text{ LL} \\ &= 1.2 \times 6.797 + 1.6 \times 3000 \\ &= 4808 \text{ lb}\end{aligned}$$

$$\begin{aligned}\text{Perimeter of bearing area for two-way shear, } b_0 &= \{4 \times (L + d')\} \\ &= \{4 \times (4.5 + 2)\} \\ &= 26 \text{ in}\end{aligned}$$

$$\begin{aligned}\text{Shear strength of concrete in two-way shear, } \phi_v V_c &= [\phi_v \times 4 \times \sqrt{f'_c} \times b_0 \times d'] \\ &= 0.75 \times 4 \times \sqrt{3500} \times 26 \times 2 \\ &= 9229.1 \text{ lb} \\ &> 4808 \text{ lb}\end{aligned}$$

13 Garage Deck Joist Design Chart

13.1 f'c = 3500 psi, Topping Thickness = 4.0"

General Data:

Unit weight of concrete = 145 pcf
 Rebar strength = 60000 psi
 Dead Load Factor = 1.2

Wheel Data:

Wheel Load = 3000 lb
 Wheel distance = 8 ft
 Deflection Factor, Δ_i LL = 180

Floor Size: 12"

Panel Size = 12"
 Live Load Factor = 1.6
 Δ_i TOTAL = 240

Dead Load = 10 psf

Span	f'c	3500 psi	LL = 50 DL = 10	
	tf	4	SS	DS
15	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
16	Bottom Reinforcement	End Spans	2#5	1#4+1#5
		Int. Spans	2#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
17	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC

18	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
19	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans		2#7
		Int. Spans		2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans		
		Int. Spans		
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
Transverse Reinf.		#4@6in OC	#4@6in OC	

	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans		
23	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans		
24	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans		
25	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	1#5+1#6
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC

Dead Load = 15 psf

Span	f'c	3500 psi	LL = 50 DL = 15	
	tf	4	SS	DS
15	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
16	Bottom Reinforcement	End Spans	2#5	1#4+1#5
		Int. Spans	2#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
17	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
18	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC

19	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans		2#7
		Int. Spans		2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans		
		Int. Spans		
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
23	Bottom Reinforcement	End Spans		
		Int. Spans		
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#5
Transverse Reinf.		#4@6in OC	#4@6in OC	

24	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans		
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	2#4
			1#4	2#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
25	Bottom Reinforcement			
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	2#4
			1#4	1#5+1#6
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC

General Data:

Unit weight of concrete = 145 pcf
 Rebar strength = 60000 psi
 Dead Load Factor = 1.2

Wheel Data:

Wheel Load = 3000 lb
 Wheel distance = 8 ft
 Deflection Factor, $\Delta_{i LL} = 360$

Floor Size: 12''

Panel Size = 12''
 Live Load Factor = 1.6
 $\Delta_{i TOTAL} = 480$

Dead Load = 10 psf

Span	f'c	3500 psi	LL = 50 DL = 10	
	tf	4	SS	DS
15	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
16	Bottom Reinforcement	End Spans	2#5	1#4+1#5
		Int. Spans	2#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
17	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC

18	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
19	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans		2#7
		Int. Spans		2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans		
		Int. Spans		
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
Transverse Reinf.		#4@6in OC	#4@6in OC	

	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans		
23	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	1#5
			1#4	2#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans		
24	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	1#5
			1#4	2#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans		
25	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	2#4
			1#4	1#5+1#6
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC

Dead Load = 15 psf

Span	f'c	3500 psi	LL = 50 DL = 15	
	tf	4	SS	DS
15	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
16	Bottom Reinforcement	End Spans	2#5	1#4+1#5
		Int. Spans	2#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
17	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
18	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC

19	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans		2#7
		Int. Spans		2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans		
		Int. Spans		
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
23	Bottom Reinforcement	End Spans		
		Int. Spans		
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#5
Transverse Reinf.		#4@6in OC	#4@6in OC	

	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans		
24	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	2#5
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans		
25	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	1#5+1#6
	Transverse Reinf.		#4@6in OC	#4@6in OC
	Longitudinal		#4@18in OC	#4@18in OC

13.2 f'c = 3500 psi, Topping Thickness = 4.5"

General Data:

Unit weight of concrete = 145 pcf
 Rebar strength = 60000 psi
 Dead Load Factor = 1.2

Wheel Data:

Wheel Load = 3000 lb
 Wheel distance = 8 ft
 Deflection Factor, Δ_i LL = 180

Floor Size: 12"

Panel Size = 12"
 Live Load Factor = 1.6
 Δ_i TOTAL = 240

Dead Load = 10 psf

Span	f'c	3500 psi	LL = 50 DL = 10	
	tf	4.5	SS	DS
15	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
16	Bottom Reinforcement	End Spans	2#5	1#4+1#5
		Int. Spans	2#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
17	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

18	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
19	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans		2#7
		Int. Spans		2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC

	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans		2#7 2#7
23	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	1#5
			1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans		
24	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	1#5
			1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans		
25	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	2#4
			1#4	1#5+1#6
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

Dead Load = 15 psf

Span	f'c	3500 psi	LL = 50 DL = 15	
	tf	4.5	SS	DS
15	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
16	Bottom Reinforcement	End Spans	2#5	1#4+1#5
		Int. Spans	2#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
17	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
18	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

19	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans		2#7
		Int. Spans		2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
23	Bottom Reinforcement	End Spans		
		Int. Spans		
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#5
Transverse Reinf.		#4@5in OC	#4@5in OC	

24	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans		
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	2#4
			1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
25	Bottom Reinforcement			
	End Spans Int. Spans			
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	2#4
			1#4	1#5+1#6
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

General Data:

Unit weight of concrete = 145 pcf
 Rebar strength = 60000 psi
 Dead Load Factor = 1.2

Wheel Data:

Wheel Load = 3000 lb
 Wheel distance = 8 ft
 Deflection Factor, $\Delta_{i LL} = 360$

Floor Size: 12"

Panel Size = 12"
 Live Load Factor = 1.6
 $\Delta_{i TOTAL} = 480$

Dead Load = 10 psf

Span	f'c	3500 psi	LL = 50 DL = 10	
	tf	4.5	SS	DS
15	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
16	Bottom Reinforcement	End Spans	2#5	1#4+1#5
		Int. Spans	2#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
17	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

18	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
19	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans		2#7
		Int. Spans		2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5

23	Transverse Reinf.		#4@5in OC	#4@5in OC	
	Longitudinal		#4@18in OC	#4@18in OC	
	Bottom Reinforcement	End Spans		2#7	
		Int. Spans		2#7	
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5	
		1 st Int. Support	1#4	2#5	
	Transverse Reinf.		#4@5in OC	#4@5in OC	
	Longitudinal		#4@18in OC	#4@18in OC	
	24	Bottom Reinforcement	End Spans		
			Int. Spans		
Longitudinal Reinforcement		Exterior Supports	1#4	1#5	
		1 st Int. Support	1#4	2#5	
Transverse Reinf.		#4@5in OC	#4@5in OC		
Longitudinal		#4@18in OC	#4@18in OC		
25		Bottom Reinforcement	End Spans		
			Int. Spans		
		Longitudinal Reinforcement	Exterior Supports	1#4	2#4
			1 st Int. Support	1#4	1#5+1#6
	Transverse Reinf.		#4@5in OC	#4@5in OC	
	Longitudinal		#4@18in OC	#4@18in OC	

Dead Load = 15 psf

Span	f'c	3500 psi	LL = 50 DL = 15	
	tf	4.5	SS	DS
15	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
16	Bottom Reinforcement	End Spans	2#5	1#4+1#5
		Int. Spans	2#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
17	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
18	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

19	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans		2#7
		Int. Spans		2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
23	Bottom Reinforcement	End Spans		
		Int. Spans		
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
1 st Int. Support		1#4	2#5	

24	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans		
		Int. Spans		
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
25	Bottom Reinforcement	End Spans		
		Int. Spans		
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	1#5+1#6
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

13.3 f'c = 4000 psi, Topping Thickness = 4.0"

General Data:

Unit weight of concrete = 145 pcf
 Rebar strength = 60000 psi
 Dead Load Factor = 1.2

Wheel Data:

Wheel Load = 3000 lb
 Wheel distance = 8 ft
 Deflection Factor, $\Delta_{iLL} = 180$

Floor Size: 12"

Panel Size = 12"
 Live Load Factor = 1.6
 $\Delta_{iTOTAL} = 240$

Dead Load = 10 psf

Span	f'c	4000 psi	LL = 50 DL = 10	
	tf	4	SS	DS
15	Bottom Reinforcement	End Spans Int. Spans	1#4+1#5 1#4+1#5	1#4+1#5 1#4+1#5
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4 1#4	1#4 1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans	2#5 2#5	1#4+1#5 1#4+1#5
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4 1#4	1#4 1#5
16	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans	2#7 2#7	2#7 2#7
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4 1#4	1#5 1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

18	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
19	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC

23	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
Longitudinal		#4@18in OC	#4@18in OC	
24	Bottom Reinforcement	End Spans		2#7
		Int. Spans		2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
25	Bottom Reinforcement	End Spans		
		Int. Spans		
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

Dead Load = 15 psf

Span	f'c	4000 psi	LL = 50 DL = 15	
	tf	4	SS	DS
15	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
16	Bottom Reinforcement	End Spans	2#5	1#4+1#5
		Int. Spans	2#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
17	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
18	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

19	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
23	Bottom Reinforcement	End Spans		2#7
		Int. Spans		2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#5
Transverse Reinf.		#4@5in OC	#4@5in OC	

24	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans		2#7
		Int. Spans		2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
Longitudinal		#4@18in OC	#4@18in OC	
25	Bottom Reinforcement	End Spans		
		Int. Spans		
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	1#5+1#6
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

General Data:

Unit weight of concrete = 145 pcf
 Rebar strength = 60000 psi
 Dead Load Factor = 1.2

Wheel Data:

Wheel Load = 3000 lb
 Wheel distance = 8 ft
 Deflection Factor, $\Delta_{i LL} = 360$

Floor Size: 12''

Panel Size = 12''
 Live Load Factor = 1.6
 $\Delta_{i TOTAL} = 480$

Dead Load = 10 psf

Span	f'c	4000 psi	LL = 50 DL = 10	
	tf	4	SS	DS
15	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
16	Bottom Reinforcement	End Spans	2#5	1#4+1#5
		Int. Spans	2#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
17	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

18	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
19	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC

23	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
Longitudinal		#4@18in OC	#4@18in OC	
24	Bottom Reinforcement	End Spans		2#7
		Int. Spans		2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
25	Bottom Reinforcement	End Spans		
		Int. Spans		
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

Dead Load = 15 psf

Span	f'c	4000 psi	LL = 50 DL = 15	
	tf	4	SS	DS
15	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
16	Bottom Reinforcement	End Spans	2#5	1#4+1#5
		Int. Spans	2#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
17	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
18	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

19	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans	2#7	2#7
		Int. Spans	2#7	2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
23	Bottom Reinforcement	End Spans		2#7
		Int. Spans		2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#5

24	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans		2#7
		Int. Spans		2#7
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
25	Bottom Reinforcement	End Spans		
		Int. Spans		
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	1#5+1#6
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

13.4 f'c = 4000 psi, Topping Thickness = 4.5"

General Data:

Unit weight of concrete = 145 pcf
 Rebar strength = 60000 psi
 Dead Load Factor = 1.2

Wheel Data:

Wheel Load = 3000 lb
 Wheel distance = 8 ft
 Deflection Factor, $\Delta_{iLL} = 180$

Floor Size: 12"

Panel Size = 12"
 Live Load Factor = 1.6
 $\Delta_{iTOTAL} = 240$

Dead Load = 10 psf

Span	f'c	4000 psi	LL = 50 DL = 10	
	tf	4.5	SS	DS
15	Bottom Reinforcement	End Spans Int. Spans	1#4+1#5 1#4+1#5	1#4+1#5 1#4+1#5
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4 1#4	1#4 1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans	1#4+1#5 1#4+1#5	1#4+1#5 1#4+1#5
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4 1#4	1#4 1#5
16	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans	1#7+1#8 1#7+1#8	1#7+1#8 1#7+1#8
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4 1#4	1#5 1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

18	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
19	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
Transverse Reinf.		#4@5in OC	#4@5in OC	

23	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans	1#7+1#8	1#7+1#8
			1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	1#5
			1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
Longitudinal		#4@18in OC	#4@18in OC	
24	Bottom Reinforcement	End Spans Int. Spans	1#7+1#8	1#7+1#8
			1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	1#5
			1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
25	Bottom Reinforcement	End Spans Int. Spans		1#7+1#8
				1#7+1#8
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	2#4
			1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

Dead Load = 15 psf

Span	f'c	4000 psi	LL = 50 DL = 15	
	tf	4.5	SS	DS
15	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
16	Bottom Reinforcement	End Spans	2#5	1#4+1#5
		Int. Spans	2#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
17	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
18	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

19	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
23	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#5
Transverse Reinf.		#4@5in OC	#4@5in OC	

24	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans		1#7+1#8
		Int. Spans		1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
Longitudinal		#4@18in OC	#4@18in OC	
25	Bottom Reinforcement	End Spans		1#7+1#8
		Int. Spans		1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	1#5+1#6
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

General Data:

Unit weight of concrete = 145 pcf
 Rebar strength = 60000 psi
 Dead Load Factor = 1.2

Wheel Data:

Wheel Load = 3000 lb
 Wheel distance = 8 ft
 Deflection Factor, Δ_i LL = 360

Floor Size: 12"

Panel Size = 12"
 Live Load Factor = 1.6
 Δ_i TOTAL = 480

Dead Load = 10 psf

Span	f'c	4000 psi	LL = 50 DL = 10	
	tf	4.5	SS	DS
15	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
16	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
17	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

18	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
19	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
Transverse Reinf.		#4@5in OC	#4@5in OC	

23	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans Int. Spans	1#7+1#8	1#7+1#8
			1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	1#5
			1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
Longitudinal		#4@18in OC	#4@18in OC	
24	Bottom Reinforcement	End Spans Int. Spans	1#7+1#8	1#7+1#8
			1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	1#5
			1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
25	Bottom Reinforcement	End Spans Int. Spans		1#7+1#8
				1#7+1#8
	Longitudinal Reinforcement	Exterior Supports 1 st Int. Support	1#4	2#4
			1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

Dead Load = 15 psf

Span	f'c	4000 psi	LL = 50 DL = 15	
	tf	4.5	SS	DS
15	Bottom Reinforcement	End Spans	1#4+1#5	1#4+1#5
		Int. Spans	1#4+1#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
16	Bottom Reinforcement	End Spans	2#5	1#4+1#5
		Int. Spans	2#5	1#4+1#5
	Longitudinal Reinforcement	Exterior Supports	1#4	1#4
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
17	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
18	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC

19	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
20	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#4
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
21	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
22	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	1#4+1#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
	Longitudinal		#4@18in OC	#4@18in OC
23	Bottom Reinforcement	End Spans	1#7+1#8	1#7+1#8
		Int. Spans	1#7+1#8	1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	1#5
		1 st Int. Support	1#4	2#5
Transverse Reinf.		#4@5in OC	#4@5in OC	

24	Longitudinal		#4@18in OC	#4@18in OC
	Bottom Reinforcement	End Spans		1#7+1#8
		Int. Spans		1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	2#5
	Transverse Reinf.		#4@5in OC	#4@5in OC
Longitudinal		#4@18in OC	#4@18in OC	
25	Bottom Reinforcement			1#7+1#8
	End Spans			1#7+1#8
	Int. Spans			1#7+1#8
	Longitudinal Reinforcement	Exterior Supports	1#4	2#4
		1 st Int. Support	1#4	1#5+1#6
	Transverse Reinf.		#4@5in OC	#4@5in OC
Longitudinal		#4@18in OC	#4@18in OC	

Notes

- Shaded portion value shows that joists are provide with shear reinforcement w/ #3 rebar single leg @ 5" O.C.
- Blank Cells indicates that the joists are failing in deflection.